## SLIDES

SERIES SIP, SHP, SJP \& STP RAIL BEARING


Series SJP

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## ORDERING DATA: SERIES SIP RAIL BEARING SLIDES

TO ORDER SPECIFY:
Product, Series, Type, Design No., Size, Travel, and Options.


| PART NO. | DESCRIPTION |
| :---: | :--- |
| $67902-1-02$ | NPN (Sink) or PNP (Source) DC Reed, 2 m cable |
| 67902-1-05 | NPN (Sink) or PNP (Source) DC Reed, 5 m cable |
| $67903-1-02$ | NPN (Sink) DC Solid State, 2 m cable |
| $67903-1-05$ | NPN (Sink) DC Solid State, 5 m cable |
| $67904-1-02$ | PNP (Source) DC Solid State, 2 m cable |
| $67904-1-05$ | PNP (Source) DC Solid State, 5 m cable |
| $67922-1$ | NPN (Sink) or PNP (Source) DC Reed, Quick Connect |
| $67923-1$ | NPN (Sink) DC Solid State, Quick Connect |
| 67924-1 | PNP (Source) DC Solid State, Quick Connect |
| $63549-02$ | 2 m Cordset with Quick Connect |
| $63549-05$ | 5 m Cordset with Quick Connect |

NOTE:

* Consult PHD for additional bore sizes and travel increments.



## BENEFITS: SERIES SIP RAIL BEARING SLIDES

## BENEFITS

- Series SIP Slides use rail bearing technology to provide smooth, precise movement with high accuracy within confined spaces.
- Available in three bore sizes with a choice of three travel lengths each.
- Standard internal shock pads eliminate metal to metal contact; reducing noise and end-of-travel impact forces.
- Standard Series SIP Slide feature mounting holes on the end and bottom of the body.
- The slide body incorporates switch slots for convenient mounting of PHD's Series 67904 mm reed and solid state switches. Magnet option (-M) is required when using Series 6790 Switches.
- Series SIP Slides offer optional 5 mm of travel adjustment on extend (-AE) or retract (-AR). Specify -AE option for extend travel adjustment, -AR for retract travel adjustment, or -AE-AR for both.

| SPECIFICATIONS | BORE SIZE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | $\mathrm{mm}$ |  |  |  |  |
| POWER SOURCE MAX. OPERATING PRESSURE OPERATING TEMPERATURERANGE | $\begin{aligned} & \text { Integral pneumatic cylinder } \\ & 100 \mathrm{psi}[7 \mathrm{bar}] \\ & -20^{\circ} \text { to } 180^{\circ} \mathrm{F}\left[-29^{\circ} \text { to } 82^{\circ} \mathrm{C}\right] \end{aligned}$ |  |  |  |  |  |
| TRAVES | $\begin{gathered} \hline .394 \\ .984 \\ 1.969 \\ \hline \end{gathered}$ | $\begin{aligned} & 10 \\ & 25 \\ & 50 \\ & \hline \end{aligned}$ | $\begin{gathered} .984 \\ 1.969 \\ 2.953 \\ \hline \end{gathered}$ | $\begin{aligned} & 25 \\ & 50 \\ & 75 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline .984 \\ 1.969 \\ 2.953 \\ \hline \end{gathered}$ | $\begin{aligned} & 25 \\ & 50 \\ & 75 \\ & \hline \end{aligned}$ |
| STANDARD ÆATURES BEARINGS <br> BODY <br> TOOL PLATE | Multiple port positions, dual mounting positions <br> Stainless steel ground rail bearing system with recirculating ball bearings <br> Anodized aluminum alloy <br> Anodized aluminum alloy |  |  |  |  |  |

FORCE TABLE

|  | SIZE 12 |  | SIZE 16 |  | SIZE 20 |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTION | $\mathbf{l b} / \mathbf{p s i}$ |  | N/bar | lb/psi | N/bar | lb/psi |
| N/bar |  |  |  |  |  |  |
| EXIEND | .176 | 11.4 | .314 | 20.3 | .486 | 31.4 |
| REIRACT | .133 | 8.6 | .270 | 17.4 | .409 | 26.4 |

## DIMENSIONS: SERIES SIP RAIL BEARING SLIDES




## NOTES:

1) DESIGNATED \& IS CENIERLINE OF UNIT
2) MEIRICINFORMATION SHOWNIN [ ]
3) CIRCLED NUMBERS INDICATE POSITION CALLOUT

## ENGINEERING DATA: SERIES SIP RAIL BEARING SLIDES

## PRESSURE RATINGS

All Series SIP Slides have an operating pressure range of 20 psi minimum to 100 psi maximum [ 1.4 to 6.9 bar ]. Maximum life will be achieved when pressure and velocity are no greater than necessary for proper operation. External flow controls are recommended. Series SIP Slides feature standard pneumatic ports on the end and both sides of the slide body, and are provided with the end ports ready for use and the side ports plugged with set screws and thread sealant.

## OPERATING TEMPERATURE

Series SIP Slides are designed for use in temperatures between $-20^{\circ}$ to $180^{\circ} \mathrm{F}\left[-29^{\circ}\right.$ to $\left.82^{\circ} \mathrm{C}\right]$. For temperatures outside this range, consult PHD.

## SEALS

Series SIP Slides utilize urethane and Nitrile seals which are compatible with standard paraffin-based lubrication oils used for pneumatic cylinders. For compatibility with other fluids, consult PHD.

## LUBRICATION

All units are prelubricated at the factory for service under normal operating conditions. Slides are designed and tested with non-lubricated air. However, the use of lubricated air will extend life.

## MATERIAL SPECIFICATIONS

The slide housing and tool plate are anodized aluminum alloy. Linear rail and bearings are hardened and ground stainless steel.

## MAINTENANCE

Common with most PHD products, these slides are fully field repairable. Repair kits and main structural components are available as needed for extended service life.

## TOTAL TRAVEL LENGTH AND WEIGHT

For standard units the tolerance of nominal travel lengths is $+.039 /-.000[+1 \mathrm{~mm} /-0 \mathrm{~mm}]$. See Options section of catalog for details regarding units with travel adjustment option (-AE or -AR).

| SIZE | NOMINAL <br> TRAVEL |  | UNIT |  |
| :---: | :---: | :---: | :---: | :---: |
|  | mm | BASE WEIGHT |  |  |
|  | kg |  |  |  |
| 12 | $(.394)$ | 10 | .30 | .14 |
|  | $(.984)$ | 25 | .35 | .16 |
|  | $(1.969)$ | 50 | .46 | .21 |
| 16 | $(1.984)$ | 25 | .71 | .32 |
|  | $(1.969)$ | 50 | .88 | .40 |
|  | $(2.953)$ | 75 | 1.04 | .47 |
| 20 | $(.984)$ | 25 | 1.04 | .47 |
|  | $(1.969)$ | 50 | 1.26 | .57 |
|  | $(2.953)$ | 75 | 1.48 | .67 |

## MOUNTING INSTRUCTIONS

PHD recommends mounting load or tooling with tool plate retracted. Support tool plate while tightening fasteners. Maximum mounting torques (for screw thread engagement of one diameter or greater):

| SIZE | in-Ib | Nm |
| :---: | :---: | :---: |
| M2 | 2.6 | 0.3 |
| M3 | 9 | 1.0 |
| M4 | 18 | 2.0 |

## ENGINEERING DATA: SERIES SIP RAIL BEARING SLIDES

## SLIDE SELECTION

There are three major factors to consider when selecting a slide: thrust capacity, dynamic moment capacity, and the allowable velocity.

## 1 THRUST CAPACITY

Use the theoretical force output table to determine if thrust is sufficient for the applied load.

## 2 DYNAMIC MOMENT CAPACITY

The Dynamic Moment Load graphs (pages 5A-7 to 5A-9) show the allowable load for the three most common mounting positions of the Series SIP Slide. Determine the distance " $x$ " from the edge of the tool plate to the load center of gravity. Use the appropriate graph for the loading condition to determine the allowable load. It is generally best to keep the center of gravity of the load as close to the slide as possible. If the application requires combined loading such as a horizontal pitch load combined with a roll load, if static loads exceed dynamic loads, or if there are other questions concerning the selection of an appropriate slide, please contact PHD's Oustomer Service Department.

3 ALLOWABLE VELOCITY
Use the allowable velocity graph to verify that the slide selected can carry the payload at the desired velocity.

ALLOWABLE LOAD VS. VELOCITY


THEOREICAL FORCE OUTPUT TABLE Ib [N]

| SIZE | DIRECTION | OPERATING PRESSUR |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} 20 \mathrm{psi} \\ \text { [1.4 bar] } \end{gathered}$ | $\begin{gathered} 30 \mathrm{psi} \\ \text { [2.1 bar] } \end{gathered}$ | $\begin{gathered} 40 \mathrm{psi} \\ \text { [2.8 bar]] } \end{gathered}$ | $\begin{gathered} 50 \mathrm{psi} \\ \text { [3.4 bar]] } \end{gathered}$ | $\begin{gathered} 60 \mathrm{psi} \\ \text { [4.1 bar]] } \end{gathered}$ | $\begin{gathered} 70 \mathrm{psi} \\ \text { [4.8 bar] } \end{gathered}$ | $\begin{gathered} 80 \mathrm{psi} \\ \text { [ } 5.5 \text { bar] } \end{gathered}$ | $\begin{gathered} 90 \mathrm{psi} \\ \text { [6.2 bar] } \end{gathered}$ | 100 psi [6.9 bar] |
| 12 | REIRACT | $\begin{gathered} 2.7 \\ {[12.0]} \end{gathered}$ | $\begin{gathered} 4.0 \\ {[17.8]} \end{gathered}$ | $\begin{gathered} 5.3 \\ {[23.6]} \end{gathered}$ | $\begin{gathered} 6.7 \\ {[29.8]} \end{gathered}$ | $\begin{gathered} 8.0 \\ {[35.6]} \end{gathered}$ | $\begin{gathered} 9.3 \\ {[41.3]} \end{gathered}$ | $\begin{gathered} 10.7 \\ {[47.6]} \end{gathered}$ | $\begin{array}{r} 12.0 \\ {[53.3]} \end{array}$ | $\begin{gathered} 13.3 \\ {[59.1]} \end{gathered}$ |
|  | EXTEND | $\begin{gathered} 3.5 \\ {[15.6]} \end{gathered}$ | $\begin{gathered} 5.3 \\ {[23.6]} \end{gathered}$ | $\begin{gathered} 7.1 \\ {[31.6]} \end{gathered}$ | $\begin{gathered} 8.8 \\ {[39.1]} \end{gathered}$ | $\begin{gathered} 10.6 \\ {[47.1]} \end{gathered}$ | $\begin{gathered} 12.4 \\ {[55.1]} \\ \hline \end{gathered}$ | $\begin{gathered} 14.1 \\ {[62.7]} \end{gathered}$ | $\begin{array}{r} 15.9 \\ {[70.7]} \end{array}$ | $\begin{array}{r} 17.6 \\ {[78.2]} \end{array}$ |
| 16 | REIRACT | $\begin{gathered} 5.4 \\ {[24.0]} \end{gathered}$ | $\begin{gathered} 8.1 \\ {[36.0]} \end{gathered}$ | $\begin{array}{r} 10.8 \\ {[48.0]} \\ \hline \end{array}$ | $\begin{gathered} 13.5 \\ {[60.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 16.2 \\ {[72.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 18.9 \\ {[84.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 21.6 \\ {[96.0]} \end{gathered}$ | $\begin{gathered} 24.3 \\ {[108.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 27.0 \\ {[120.0]} \end{gathered}$ |
|  | EXTEND | $\begin{gathered} 6.3 \\ {[28.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 9.4 \\ {[41.8]} \end{gathered}$ | $\begin{array}{r} 12.5 \\ {[55.6]} \\ \hline \end{array}$ | $\begin{gathered} 15.7 \\ {[69.8]} \end{gathered}$ | $\begin{gathered} 18.8 \\ {[83.6]} \end{gathered}$ | $\begin{gathered} 22.0 \\ {[97.8]} \end{gathered}$ | $\begin{gathered} 25.1 \\ {[111.6]} \\ \hline \end{gathered}$ | $\begin{gathered} 28.2 \\ {[125.3]} \end{gathered}$ | $\begin{gathered} 31.4 \\ {[139.6]} \end{gathered}$ |
| 20 | REIRACT | $\begin{gathered} 8.2 \\ {[37.0]} \end{gathered}$ | $\begin{gathered} 12.3 \\ {[55.4]} \end{gathered}$ | $\begin{array}{r} 16.4 \\ {[73.9]} \end{array}$ | $\begin{gathered} 20.5 \\ {[89.8]} \end{gathered}$ | $\begin{gathered} 24.5 \\ {[108.2]} \end{gathered}$ | $\begin{gathered} 28.6 \\ {[126.7]} \end{gathered}$ | $\begin{gathered} 32.7 \\ {[145.2]} \\ \hline \end{gathered}$ | $\begin{gathered} 36.8 \\ {[163.7]} \end{gathered}$ | $\begin{gathered} 40.9 \\ {[182.2]} \end{gathered}$ |
|  | EXTEND | $\begin{gathered} 9.7 \\ {[44.0]} \end{gathered}$ | $\begin{gathered} 14.6 \\ {[65.9]} \end{gathered}$ | $\begin{gathered} 19.4 \\ {[87.9]} \end{gathered}$ | $\begin{gathered} 24.3 \\ {[106.8]} \end{gathered}$ | $\begin{gathered} 29.2 \\ {[128.7]} \end{gathered}$ | $\begin{gathered} 34.0 \\ {[150.7]} \end{gathered}$ | $\begin{gathered} 38.9 \\ {[172.7]} \end{gathered}$ | $\begin{gathered} 43.7 \\ {[194.7]} \end{gathered}$ | $\begin{gathered} 48.6 \\ {[216.7]} \end{gathered}$ |

MAXIMUM DYNAMIC HORIZONTAL PITCH MOMENT LOADS



## ENGINEERING DATA:' SERIES SIP SIZE 16, DYNAMIC MOMENT LOADS




MAXIMUM DYNAMIC VERTICAL PITCH MOMENT LOADS


MAXIMUM DYNAMIC ROLL MOMENT LOADS



## $\begin{array}{cr}-\quad \text { SIP16x25 } \\ - \text { - } & \text { SIP16x50 } \\ \cdots . . . . . . . & \text { SIP16x75 }\end{array}$



- SIP16x25
-     -         - SIP16x50
........... SIP16x75

—— SIP16x25, tool plate"0"
-     -         - SIP16x50, tool plate"0"
............ SIP16x75, tool plate"0"
- SIP16x25, rear pattern
-     -         - SIP16x50, rear pattern
............ SIP16x75, rear pattern

MAXIMUM DYNAMIC HORIZONTAL PITCH MOMENT LOADS


MAXIMUM DYNAMIC VERTICAL PITCH MOMENT LOADS


MAXIMUM DYNAMIC ROLL MOMENT LOADS



## OPTIONS: SERIES SIP RAIL BEARING SLIDES

## M

MAGNET FOR PHD SERIES 6790 REED AND SOLID STATE SWITCHES

This option equips the unit with a magnetic piston for use with PHD's Series 6790 Switch. The switch housing is contained by the slide housing and provides a very compact switch design. The switches mount easily into two small grooves located on the side of the slide housing and are locked into place with a set screw.

| LEITER | SIZE 12 |  | SIZE 16 |  | SIZE 20 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIM | in | mm | in | mm | in | mm |
| A | 0.689 | 17.5 | 0.933 | 23.7 | 1.122 | 28.5 |
| B | 0.492 | 12.5 | 0.551 | 14 | 0.591 | 15 |



SERIES 6790 REED SWITCHES

| SIZE | REPEATABILITY |  | HYSTERESIS MAXIMUM |  | BANDWIDTH MIN./MAX. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | mm | in | mm | in | mm |
| 12 | +/-. 005 | +/-. 13 | 0.060 | 1.5 | . $380 / .400$ | 9.7/10.2 |
| 16 | +/-. 005 | +/-. 13 | 0.080 | 2.0 | .220/.350 | 5.6/8.9 |
| 20 | +/-. 005 | +/-. 13 | 0.060 | 1.5 | .335/. 750 | 8.5/19.0 |

SERIES 6790 SOLID STATE SWITCHES

| SIZE | REPEATABILITY |  | HYSTERESIS MAXIMUM |  | BANDWIDTH MIN./MAX. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | mm | in | mm | in | mm |
| 12 | +/-. 005 | +/-. 13 | 0.060 | 1.5 | .335/.630 | 8.5/16.0 |
| 16 | +/-. 005 | +/-. 13 | 0.080 | 2.0 | .170/.490 | 4.3/12.4 |
| 20 | +/-. 005 | +/-. 13 | 0.060 | 1.5 | .280/.670 | 7.1/17.0 |

## AE <br> TRAVEL ADJUSTMENT ON EXTEND

This option provides up to 5 mm of travel on extend. Travel adjustment is made using a spanner wrench or similar tool to engage the slots in the cartridge and rotating the cartridge to the desired position. Rotating the cartridge clockwise reduces the travel. Normal shock pad operation is maintained regardless of cartridge position. Travel adjustment has internal stops, preventing loss of components. The -AE option may be used in conjunction with the -AR option to provide travel adjustment at both ends of travel.

CARTRIDGE SLOT DETAIL


|  | "A" |  | "B" |  | "C" ROD |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZT | SLOT WIDTH |  | MAX TOOL DIA |  | CLEARANCE DIA |  | SLOT DEPTH |  |
| in | mm | in | mm | in | mm | in | mm |  |
| 12 | .062 | 1.6 | .450 | 11.4 | .215 | 5.5 | .030 | .8 |
| 16 | .062 | 1.6 | .600 | 15.2 | .362 | 9.2 | .060 | 1.5 |
| 20 | .062 | 1.6 | .817 | 20.8 | .478 | 12.1 | .060 | 1.5 |

## AR <br> TRAVEL ADJUSTMENT ON RETRACT

This option provides up to 5 mm of travel on retract. Travel adjustment is made using a flat-bladed screwdriver or similar tool to engage the slot in the bore plug and rotating the bore plug to the desired position. Rotating the bore plug clockwise reduces the travel. Normal shock pad operation is maintained regardless of bore plug position. Travel adjustment has internal stops, preventing loss of components. The-AR option may be used in conjunction with the -AE option to provide travel adjustment at both ends of travel.

BORE PLUG SLOT DETAIL


|  | "A" SLOT WIDTH |  | "B" MAX TOOL DIA |  | SLOT DEPTH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | in | mm | in | mm | in | mm |
| 12 | .062 | 1.6 | .450 | 11.4 | .030 | .8 |
| 16 | .062 | 1.6 | .600 | 15.2 | .060 | 1.5 |
| 20 | .062 | 1.6 | .817 | 20.8 | .060 | 1.5 |

## TO ORDER SPECIFY：

Product，Series，Bearing Type，Design
No．，Size，Travel，and Option．


| PART NO． | DESCRIPTION |
| :---: | :--- |
| $67902-1-02$ | NPN（Sink）or PNP（Source）DC Reed， 2 m cable |
| $67902-1-05$ | NPN（Sink）or PNP（Source）DC Reed， 5 m cable |
| $67903-1-02$ | NPN（Sink）DC Solid State， 2 m cable |
| $67903-1-05$ | NPN（Sink）DC Solid State， 5 m cable |
| $67904-1-02$ | PNP（Source）DC Solid State， 2 m cable |
| $67904-1-05$ | PNP（Source）DC Solid State， 5 m cable |
| 67922－1 | NPN（Sink）or PNP（Source）DC Reed，Quick Connect |
| $67923-1$ | NPN（Sink）DC Solid State，Quick Connect |
| 67924－1 | PNP（Source）DC Solid State，Quick Connect |
| 63549－02 | 2 m Cordset with Quick Connect |
| 63549－05 | 5 m Cordset with Quick Connect |

## BENEFITS: SERIES SHP SLIDES WITH RAIL BEARING

## BENEFITS

- Series SHP Slides use rail bearing technology to provide smooth, precise movement within confined spaces.
- Available in three bore sizes and five travel lengths.
- Standard travel adjustments for both extend and retract positions are conveniently located on the back of the slide. Integrated shock pads provide shock reduction throughout the full range of travel adjustment.
- Available in both imperial and metric versions for applications in worldwide markets.

- Standard Series SHP Slides provide multiple mounting options for maximum flexibility. Bodies feature mounting holes on sides, end, and bottom. Tool plates feature mounting on top and end.
- Standard dowel holes are provided on the body and both end and top tool plate mounting positions for precise mounting and attachment of tooling.
- Slide housing provides dual switch slots on either side for convenient mounting of PHD's Series 67904 mm Reed and Solid State switches. Magnet option ( -M ) is required when using switches.
Bore Plug-
on the
e
slots on
of PHD's
State
quired when


| SPECIFICATIONS | BORE SIZE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | mm |  |  |  |  |
| POWER SOURCE <br> MAX. OPERATINGPRESSURE OPERATING TEMPERATURE RANGE | $\begin{aligned} & \text { Integral pneumatic cylinder } \\ & 100 \mathrm{psi}[6.9 \mathrm{bar}] \\ & -20^{\circ} \text { to } 180^{\circ} \mathrm{F}\left[-29^{\circ} \text { to } 82^{\circ} \mathrm{C}\right] \end{aligned}$ |  |  |  |  |  |
| TRAVES | $\begin{gathered} .79 \\ 1.57 \end{gathered}$ | $\begin{aligned} & 20 \\ & 40 \end{aligned}$ | $\begin{gathered} .79 \\ 1.57 \end{gathered}$ | $\begin{aligned} & 20 \\ & 40 \end{aligned}$ | $\begin{gathered} \hline .59 \\ 1.38 \\ 2.17 \\ \hline \end{gathered}$ | $\begin{aligned} & 15 \\ & 35 \\ & 55 \\ & \hline \end{aligned}$ |
| TRAVE ADJUSTMENTS STANDARD ÆATURES BEARINGS BODY TOOL PLATE | Standard on both extend and retract <br> Multiple port positions, multiple mounting positions, dowel pin holes Stainless steel ground rail bearing system with recirculating ball bearings <br> Anodized aluminum alloy <br> Anodized aluminum alloy |  |  |  |  |  |


| FORCE TABLE |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SIZE 08 |  | SIZE 12 |  | SIZE 16 |  |
| DIRECTION | lb/psi | N/B | $\mathbf{l b} / \mathbf{p s i}$ | N/B | lb/psi | N/B |
| EXTEND | .079 | 5.1 | .176 | 11.4 | .314 | 20.3 |
| REIRACT | .060 | 3.9 | .133 | 8.6 | .270 | 17.4 |

## DIMENSIONS: SERIES SHP SLIDES - SIZE 08



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## DIMENSIONS: SERIES SHP SLIDES - SIZES 12 \& 16



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## ENGINEERING DATA: sERIES SHP SLIDES

## PRESSURE RATINGS

All Series SHP Slides have an operating pressure range of 20 psi minimum to 100 psi maximum [ 1.4 to 6.9 bar]. For longest slide life it is recommended that pressure and velocity be no greater than necessary for proper operation. Series SHP Slides incorporate internal orifices to help limit velocities. However, external flow controls are recommended at higher pressures or if slide operation results in strong impact loads at ends of travel. Series SHP Slides feature standard pneumatic ports on the end and both sides of the slide body, and are provided with the end ports ready for use and the side ports plugged with set screws and thread sealant.

## OPERATING TEMPERATURE

Series SHP Slides are designed for use in temperatures between $20^{\circ}$ to $180^{\circ} \mathrm{F}\left[-6^{\circ}\right.$ to $82^{\circ} \mathrm{C}$. For temperatures outside this range, consult PHD.

## SEALS

Series SHP Slides utilize urethane and Nitrile seals which are compatible with standard paraffin-based lubrication oils used for pneumatic cylinders. For compatibility with other fluids, consult PHD.

## LUBRICATION

All units are pre-lubricated at the factory for service under normal operating conditions. Slides are designed and tested with non-lubricated air. However, the use of lubricated air will extend life.

## MATERIAL SPECIFICATIONS

The slide housing and tool plate are anodized aluminum alloy. Linear rail and bearings are hardened and ground stainless steel.

## MAINTENANCE

In common with most PHD products, these slides are fully field repairable. Repair kits and main structural components are available as needed for extended service life.

| UNIT WEIGHT |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| SIZE | TRAVEL |  | WEIGHT |  |
|  | mm | lb | kg |  |
|  | .79 | 20 | .20 | .09 |
|  | 1.57 | 40 | .26 | .12 |
| 12 | .79 | 20 | .38 | .17 |
|  | 1.57 | 40 | .48 | .22 |
| 16 | .59 | 15 | .56 | .25 |
|  | 1.38 | 35 | .71 | .32 |
|  | 2.17 | 55 | .85 | .39 |

## TRAVEL ADJUSTMENT

Standard Series SHP Slides provide travel adjustment in both the retract and extend directions. Travel adjustments are made using a small flat bladed or standard screwdriver via the adjustment holes located on the back of the slide. Series SHP Slides are designed to provide nominal travel. Using the travel adjustment screws allows reducing either the extend or retract travel by . 394 in [ 10 mm ] ( 5 mm for SHP08).

Travel adjustment requires a small flat bladed screwdriver with a minimum shank length and diameter as shown in the table below. Blade thickness should not exceed .030 in [. 75 mm ]. Travel adjustments should not be adjusted beyond positions shown in illustration. Loss of components or damage to the mechanism may occur if adjusted beyond the recommended limits.


## ENGINEERING DATA: SERIES SHP SLIDES

## SLIDE SELECTION

There are three major factors to consider when selecting a slide: thrust capacity, allowable mass, and dynamic moment capacity.

1 THRUST CAPACITY
Use the theoretical output table to determine if thrust is sufficient for the applied load.

2 MAXIMUM PAYLOAD CAPACITY
All Series SHP Slides come standard with end of travel shock pads. However, these shock pads are limited in the amount of energy that they can dissipate. Therefore, the slides have a maximum payload limit. Use the allowable velocity graph to verify that the slide can carry the payload at the desired velocity.

## 3 DYNAMIC MOMENT CAPACITY

The Dynamic Moment Load graphs show the allowable load for the three most common mounting positions of the Series SHP Slide. Determine the distance " $x$ " from the edge of the tool plate to the load center of gravity. Use the graph appropriate for the loading condition to determine the allowable load. It is generally best to keep the load center of gravity as close to the slide as possible. (See next page for graphs.) If the application requires combined loading such as a horizontal pitch load combined with a roll load, if static loads exceed dynamic loads, or if there are other questions concerning the selection of an appropriate slide, please contact PHD's Oustomer Service Department.


SIZE 08


THEORETICAL OUTPUT TABLE Ib [N]

| SIZE | DIRECTION | OPERATING PRESSURE |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} 20 \mathrm{psi} \\ \text { [1.4 bar] } \end{gathered}$ | $\begin{gathered} 30 \mathrm{psi} \\ {[2.1 \mathrm{bar}]} \end{gathered}$ | $\begin{gathered} 40 \mathrm{psi} \\ \text { [2.8 bar] } \end{gathered}$ | $\begin{gathered} 50 \mathrm{psi} \\ {[3.4 \mathrm{bar}]} \end{gathered}$ | 60 psi <br> [4.1 bar] | 70 psi <br> [4.8 bar] | $\begin{gathered} 80 \mathrm{psi} \\ \text { [5.5 bar]] } \end{gathered}$ | 90 psi $[6.2 \mathrm{bar}]$ | $\begin{gathered} 100 \mathrm{psi} \\ {[6.9 \mathrm{bar}]} \end{gathered}$ |
| 08 | REIRACT | $\begin{gathered} 1.2 \\ {[5.3]} \\ \hline \end{gathered}$ | $\begin{gathered} 1.8 \\ {[8.0]} \end{gathered}$ | $\begin{gathered} 2.4 \\ {[10.7]} \end{gathered}$ | $\begin{gathered} 3.0 \\ {[13.3]} \end{gathered}$ | $\begin{gathered} 3.6 \\ {[16.0]} \end{gathered}$ | $\begin{gathered} 4.2 \\ {[18.7]} \end{gathered}$ | $\begin{gathered} 4.8 \\ {[21.3]} \end{gathered}$ | $\begin{gathered} 5.4 \\ {[24.0]} \end{gathered}$ | $\begin{gathered} 6.0 \\ {[26.7]} \\ \hline \end{gathered}$ |
|  | EXTEND | $\begin{gathered} 1.6 \\ {[7.1]} \\ \hline \end{gathered}$ | $\begin{gathered} 2.4 \\ {[10.7]} \end{gathered}$ | $\begin{gathered} 3.1 \\ {[13.8]} \end{gathered}$ | $\begin{gathered} 3.9 \\ {[17.3]} \end{gathered}$ | $\begin{gathered} 4.7 \\ {[20.9]} \end{gathered}$ | $\begin{gathered} 5.5 \\ {[24.4]} \end{gathered}$ | $\begin{gathered} 6.3 \\ {[28.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 7.1 \\ {[31.6]} \end{gathered}$ | $\begin{gathered} 7.9 \\ {[35.1]} \end{gathered}$ |
| 12 | REIRACT | $\begin{gathered} 2.7 \\ {[12.0]} \end{gathered}$ | $\begin{gathered} 4.0 \\ {[17.8]} \end{gathered}$ | $\begin{gathered} 5.3 \\ {[23.6]} \end{gathered}$ | $\begin{gathered} 6.7 \\ {[29.8]} \end{gathered}$ | $\begin{gathered} 8.0 \\ {[35.6]} \end{gathered}$ | $\begin{gathered} 9.3 \\ {[41.3]} \end{gathered}$ | $\begin{gathered} 10.7 \\ {[47.6]} \end{gathered}$ | $\begin{gathered} 12.0 \\ {[53.3]} \end{gathered}$ | $\begin{gathered} 13.3 \\ {[59.1]} \end{gathered}$ |
|  | EXTEND | $\begin{gathered} 3.5 \\ {[15.6]} \end{gathered}$ | $\begin{gathered} 5.3 \\ {[23.6]} \end{gathered}$ | $\begin{gathered} 7.1 \\ {[31.6]} \end{gathered}$ | $\begin{gathered} 8.8 \\ {[39.1]} \end{gathered}$ | $\begin{gathered} 10.6 \\ {[47.1]} \end{gathered}$ | $\begin{gathered} 12.4 \\ {[55.1]} \\ \hline \end{gathered}$ | $\begin{array}{r} 14.1 \\ {[62.7]} \\ \hline \end{array}$ | $\begin{array}{r} 15.9 \\ {[70.7]} \\ \hline \end{array}$ | $\begin{gathered} 17.6 \\ {[78.2]} \end{gathered}$ |
| 16 | REIRACT | $\begin{gathered} 5.4 \\ {[24.0]} \end{gathered}$ | $\begin{gathered} 8.1 \\ {[36.0]} \end{gathered}$ | $\begin{gathered} 10.8 \\ {[48.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 13.5 \\ {[60.0]} \end{gathered}$ | $\begin{gathered} 16.2 \\ {[72.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 18.9 \\ {[84.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 21.6 \\ {[96.0]} \\ \hline \end{gathered}$ | $\begin{gathered} 24.3 \\ {[108.0]} \end{gathered}$ | $\begin{gathered} 27.0 \\ {[120.0]} \\ \hline \end{gathered}$ |
|  | EXTEND | $\begin{gathered} 6.3 \\ {[28.0]} \end{gathered}$ | $\begin{gathered} 9.4 \\ {[41.8]} \end{gathered}$ | $\begin{gathered} 12.5 \\ {[55.6]} \end{gathered}$ | $\begin{gathered} 15.7 \\ {[69.8]} \end{gathered}$ | $\begin{gathered} 18.8 \\ {[83.6]} \end{gathered}$ | $\begin{gathered} 22.0 \\ {[97.8]} \end{gathered}$ | $\begin{gathered} 25.1 \\ {[111.6]} \end{gathered}$ | $\begin{gathered} 28.2 \\ {[125.3]} \end{gathered}$ | $\begin{gathered} 31.4 \\ {[139.6]} \end{gathered}$ |


| UNIT | TRAVEL TIME |
| :---: | :---: |
| SHP08×20 | 0.1 |
| SHP08×40 | 0.18 |
| SHP12x20 | 0.18 |
| SHP12x40 | 0.22 |
| SHP $16 \times 15$ | 0.15 |
| SHP16x35 | 0.2 |
| SHP16x55 | 0.25 |
| NOTES: |  |

## NOTES:

1) Travel time is in seconds from application of pressure. 2) Travel times relatively independent of pressure between 60 and 100 psi.


## MAXIMUM DYNAMIC HORIZONTAL PITCH MOMENT LOADS

## SIZE 12




## ENGINEERING DATA: sERIES SHP SLIDES

## MAXIMUM DYNAMIC ROLL MOMENT LOADS



## MAXIMUM DYNAMIC VERTICAL PITCH MOMENT LOADS



## OPTION: sERIES SHP SLIDES

## M <br> MAGNET FOR PHD SERIES 6790 MINIATURE REED AND SOLID STATE SWITCHES

This option equips the unit with a magnetic piston for use with PHD's Series 6790 Switch. The switch housing is contained by the slide housing and provides a very compact switch design. The switches mount easily into two small grooves located on the side of the slide housing and are locked into place with a set screw.

| PART NO. | DESCRIPTION |
| :---: | :--- |
| $67902-1-02$ | NPN (Sink) or PNP (Source) DC Reed, 2 m cable |
| $67902-1-05$ | NPN (Sink) or PNP (Source) DC Reed, 5 m cable |
| $67903-1-02$ | NPN (Sink) DC Solid State, 2 m cable |
| $67903-1-05$ | NPN (Sink) DC Solid State, 5 m cable |
| $67904-1-02$ | PNP (Source) DC Solid State, 2 m cable |
| $67904-1-05$ | PNP (Source) DC Solid State, 5 m cable |
| $67922-1$ | NPN (Sink) or PNP (Source) DC Reed, Quick Connect |
| $67923-1$ | NPN (Sink) DC Solid State, Quick Connect |
| $67924-1$ | PNP (Source) DC Solid State, Quick Connect |
| $63549-02$ | 2 m Cordset with Quick Connect |
| $63549-05$ | 5 m Cordset with Quick Connect |



## REED BENEFITS

- Available as 4.5-30 VDC model for simple interfacing to sequencers and programmable controllers.
- Can be used to directly drive some types of relays or valve solenoids within the switch specifications stated.

| SPECIFICATIONS | $\mathbf{6 7 9 0 2} \& \mathbf{6 7 9 2 2}$ |
| :--- | :---: |
| OPERATING PRINCIPLE | Magnetic Reed |
| ACTUATED BY | Piston Magnet |
| INPUT VOLTAGE | $4.5-30$ VDC |
| OUTPUT TYPE | Contact Cosure |
| CURRENT RATING | 50 mA Max. |
| OONTACT RESISTANCE | .1150 Om Max. |
| QNVIRONMENTAL | IP67 |
| OPERATING TEMP. | $-20^{\circ}$ to $85^{\circ} \mathrm{C}$ |

## SOLID STATE BENEFITS

- Solid state switches afford long life. Constant amplitude output allows use with most digital logic systems.
- Switch circuitry protects against voltage surges and other electrical anomalies associated with operating systems.
- Excellent switch hysteresis characteristics and symmetry.
- Offered in 4.5-30 VDC current sinking and current sourcing versions for simple interfacing to electronic system controllers.

| SPECIFICATIONS | 67903 \& $67923 \quad 67904$ \& 67924 |
| :---: | :---: |
| OPGRATING PRINCIPLE | Solid State |
| ACTUATED BY | Piston Magnet |
| INPUT VOLTAGE | 4.5-30 VDC |
| OUTPUT TYPE | NPN (Sink) PNP (Source) |
| CURRENT RATING | 50 mA . Max |
| VOLTAGE DROP | . 5 VDC |
| SWITCH BURDEN | 10 mA . Max. |
| ENVIRONMENTAL | IP67 |
| OPERATING TEMP. | $-20^{\circ}$ to $85^{\circ} \mathrm{C}$ |

MALE QUICK CONNECT DETAIL


METRIC INFORMATION SHOWN IN[ ]

63549-xx CORDSET WITH FEMALE QUICK CONNECT


## ORDERING DATA: SERIES SJP RAIL BEARING SLIDES

TO ORDER SPECIFY:
Product, Series, Bearing Type, Design No., Size, Travel, and Options.


| PART NO. | DESCRIPTION |
| :---: | :--- |
| $67902-1-02$ | NPN (Sink) or PNP (Source) DC Reed, 2 m cable |
| $67902-1-05$ | NPN (Sink) or PNP (Source) DC Reed, 5 m cable |
| 67903-1-02 | NPN (Sink) DC Solid State, 2 m cable |
| 67903-1-05 | NPN (Sink) DC Solid State, 5 m cable |
| $67904-1-02$ | PNP (Source) DC Solid State, 2 m cable |
| 67904-1-05 | PNP (Source) DC Solid State, 5 m cable |
| $67922-1$ | NPN (Sink) or PNP (Source) DC Reed, Quick Connect |
| $67923-1$ | NPN (Sink) DC Solid State, Quick Connect |
| 67924-1 | PNP (Source) DC Solid State, Quick Connect |
| $63549-02$ | 2 m Cordset with Quick Connect |
| $63549-05$ | 5 m Cordset with Quick Connect |

## NOTES:

* See page 5A-7 for use of the-MA option.
**Consult PHD for additional travel increments.


## BENEFITS:' SERIES SJP RAIL BEARING SLIDES

## BENEFITS

- This slide is designed to be an MRO drop-in. Consult PHD or your local distributor for unit compatibility.
- Series SJP Slides use rail bearing technology to provide smooth, precise movement with high accuracy within confined spaces.
- Available in three bore sizes with three travel lengths each.
- Standard internal shock pads eliminate metal to metal contact reducing noise and end-of-travel impact forces.
- Standard Series SJP Slides provide multiple mounting options for maximum flexibility. Bodies feature mounting holes on sides, end, and bottom.
- Slide body incorporates twin switch slots on both sides for convenient mounting of PHD's Series 67904 mm Reed and solid state switches. Magnet option -M is required when using Series 6790 Switches.

- Series SJP Slides can be fitted with certain competitor's switches. Magnet option -MA is required when using these switches.

| SPECIFICATIONS | BORE SIZE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\text { in } \quad \begin{aligned} & 08 \\ & \mathrm{~mm} \end{aligned}$ |  |  |  |  |
| POWER SOURCE <br> MAX. OPRATINGPRESSURE <br> OPGRATING TEMPERATURERANGE | $\begin{aligned} & \text { Integral pneumatic cylinder } \\ & 100 \text { psi [6.9 bar] } \\ & -20^{\circ} \text { to } 180^{\circ} \mathrm{F}\left[-29^{\circ} \text { to } 82^{\circ} \mathrm{C}\right] \end{aligned}$ |  |  |  |  |
| TRAVES | .394 10 <br> .591 15 <br> .984 25 | $\begin{aligned} & .591 \\ & .787 \\ & .984 \end{aligned}$ | $\begin{aligned} & 15 \\ & 20 \\ & 25 \\ & \hline \end{aligned}$ | $\begin{array}{r} .591 \\ .984 \\ 1.181 \\ \hline \end{array}$ | $\begin{aligned} & 15 \\ & 25 \\ & 30 \end{aligned}$ |
| STANDARD ÆATURES BEARINGS <br> BODY <br> TOOL PLATE | Multiple port positions, multiple mounting positions <br> Stainless steel ground rail bearing system with recirculating ball bearings <br> Anodized aluminum alloy <br> Anodized aluminum alloy |  |  |  |  |

FORCE TABLE

|  | SIZE 08 |  | SIZE 12 |  | SIZE 16 |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTION | lb/psi | N/bar | lb/psi | N/bar | lb/psi | N/bar |
| EXTEND | .079 | 5.1 | .175 | 11.3 | .314 | 20.3 |
| REIRACT | .060 | 3.9 | .132 | 8.5 | .270 | 17.4 |

## DIMENSIONS: SERIES SJP RAIL BEARING SLIDES




NOTES:

1) DESIGNATE $\&$ IS CENTERLINEOFUNIT.
2) MEIRIC INFORMATION SHOWN IN [ ].
3) CRQ_-D NUMBERS INDICATE POSITION CALLOU.

## ENGINEERING DATA: SERIES SJP RAIL BEARING SLIDES

## PRESSURE RATINGS

All Series SJP Slides have an operating pressure range of 20 psi minimum to 100 psi maximum [ 1.4 to 6.9 bar]. Maximum life will be achieved when pressure and velocity are no greater than necessary for proper operation. External flow controls are recommended. Series SJP Slides feature standard pneumatic ports on the end and both sides of the slide body, and are provided with the end ports ready for use and the side ports plugged with set screws and thread sealant.

## OPERATING TEMPERATURE

Series SJP Slides are designed for use in temperatures between $-20^{\circ}$ to $180^{\circ} \mathrm{F}\left[-29^{\circ}\right.$ to $82^{\circ} \mathrm{C}$. For temperatures outside this range, consult PHD.

## SEALS

Series SJP Slides utilize urethane and Nitrile seals which are compatible with standard paraffin-based lubrication oils used for pneumatic cylinders. For compatibility with other fluids, consult PHD.

## LUBRICATION

All units are prelubricated at the factory for service under normal operating conditions. Slides are designed and tested with non-lubricated air. However, the use of lubricated air will extend life.

## SLIDE SELECTION

There are three major factors to consider when selecting a slide: thrust capacity, dynamic moment capacity, and the allowable velocity.

1 THRUST CAPACITY
Use the theoretical force output table to determine if thrust is sufficient for the applied load.

2 DYNAMIC MOMENT CAPACITY
The Dynamic Moment Load graphs show the allowable load for the three most common mounting positions of the Series SJP Slide. Determine the distance " $x$ " from the edge of the tool plate to the load


## TOTAL TRAVEL LENGTH AND WEGGHT

Tolerance of minimum travel length is $+.039 /-.000$ [ $+1 \mathrm{~mm} /-0 \mathrm{~mm}$ ].

| SIZE | MINIMUM |  | TRAVEL |  |
| :---: | :---: | :---: | :---: | :---: |
|  | mm | BASE WEIGHT |  |  |
|  | kg |  |  |  |
| 08 | $(.394)$ | 10 | .16 | .07 |
|  | $(.591)$ | 15 | .18 | .08 |
|  | $(.984)$ | 25 | .21 | .10 |
| 12 | $(.591)$ | 15 | .32 | .15 |
|  | $(.787)$ | 20 | .35 | .16 |
|  | $(.984)$ | 25 | .39 | .18 |
| 16 | $(.591)$ | 15 | .57 | .26 |
|  | $(.984)$ | 25 | .65 | .29 |
|  | $(1.181)$ | 30 | .68 | .31 |

## MATERIAL SPECIFICATIONS

The slide housing and tool plate are anodized aluminum alloy. Linear rail and bearings are hardened and ground stainless steel.

## MAINTENANCE

In common with most PHD products, these slides are fully field repairable. Repair kits and main structural components are available as needed for extended service life.

## MOUNTING INSTRUCTIONS

PHD recommends to mount load or tooling with tool plate retracted. Support tool plate while tightening fasteners. Maximum mounting torques (for screw thread engagement of one diameter or greater):

| FASTENER SIZE | in-lb | Nm |
| :---: | :---: | :---: |
| M3 | 9 | 1 |
| M4 | 18 | 2 |
| M5 | 35 | 4 |
| *Mounting holes only, port fittings require less. |  |  |

THEORETICAL FORCE OUTPUT TABLE lb [N]

| SIZE | DIRECTION | OPERATING PRESSURE |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} 20 \mathrm{psi} \\ \text { [1.4 barl } \end{gathered}$ | $\begin{gathered} 30 \mathrm{psi} \\ \text { [2.1 bar] } \end{gathered}$ | $\begin{gathered} 40 \mathrm{psi} \\ {[2.8 \mathrm{bar}} \end{gathered}$ | $\begin{gathered} 50 \mathrm{psi} \\ \text { [3.4 bar] } \end{gathered}$ | $60 \mathrm{psi}$ [4.1 bar] | $\begin{gathered} 70 \mathrm{psi} \\ \text { [4.8 bar } \end{gathered}$ | $\begin{gathered} 80 \mathrm{psi} \\ \text { [5.5 barl } \end{gathered}$ | $\begin{gathered} 90 \mathrm{psi} \\ \text { [6.2 bar] } \end{gathered}$ | $\begin{gathered} 100 \mathrm{psi} \\ \text { [6.9 bar] } \end{gathered}$ |
| 08 | REIRACT | $1.2$ | $1.8$ | $2.4$ | $3.0$ | $3.6$ | 4.2 | $4.8$ | $5.4$ | $6.0$ |
|  | EXTEND | 1.6 | [8.0] 2.4 | $\frac{[10.7]}{3.1}$ | [13.3] 3.9 | $\frac{[16.0]}{4.7}$ | [18.7] | $\frac{[21.3]}{6.3}$ | $\frac{[24.0]}{7.1}$ | 7.9 |
|  |  | [7.1] | [10.7] | [13.8] | [17.3] | [20.9] | [24.4] | [28.0] | [31.6] | [35.1] |
| 12 | REIRACT | $2.7$ | $4.0$ | $5.3$ | $6.7$ | $8.0$ | $\begin{gathered} 9.3 \\ {[41.31} \end{gathered}$ | $10.7$ | 12.0 |  |
|  | EXTEND | 3.5 | 5.3 | 7.1 | 8.8 | 10.6 | 12.4 | 14.1 | 15.9 | 17.6 |
|  |  | [15.6] | [23.6] | [31.6] | [39.1] | [47.1] | [55.1] | [62.7] | [70.7] | [78.2] |
| 16 | REIRACT | 5.4 | 8.1 | 10.8 | 13.5 | 16.2 | 18.9 | 21.6 | 24.3 | 27.0 |
|  |  | [24.0] | [36.0] | [48.0] | [60.0] | [72.0] | [84.0] | [96.0] | [108.0] | [120.0] |
|  | EXTEND | 6.3 | 9.4 | 12.5 | 15.7 | 18.8 | 22.0 | 25.1 | 28.2 | 31.4 |
|  |  | [28.0] | [41.8] | [55.6] | [69.8] | [83.6] | [97.8] | [111.6] | [125.3] | [139.6] |

center of gravity. Use the appropriate graph for the loading condition to determine the allowable load. It is generally best to keep the center of gravity of the load as close to the slide as possible. (See next page for graphs.) If the application requires combined loading such as a horizontal pitch load combined with a roll load, if static loads exceed dynamic loads, or if there are other questions concerning the selection of an appropriate slide, please contact PHD's Customer Service Department.

## 3 ALLOWABLE VELOCITY

Use the allowable velocity graph at left to verify that the slide selected can carry the payload at the desired velocity.

## ENGINEERING DATA: SERIES SJP RAIL BEARING SLIDES

MAXIMUM DYNAMIC HORIZONTAL PITCH MOMENT LOADS


SIZE 08




## OPTIONS: SERIES SJP RAIL BEARING SLIDES

## M <br> MAGNET FOR PHD SERIES 6790 REED AND SOLID STATE SWITCHES

This option equips the unit with a magnetic piston for use with PHD's Series 6790 Switch. The switch housing is contained by the slide housing and provides a very compact switch design. The switches mount easily into two small grooves located on the side of the slide housing and are locked into place with a set screw.


| LETTER | SIZE 08 |  | SIZE 12 |  | SIZE 16 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIM | in | mm | in | mm | in | mm |
| A | 0.496 | 12.6 | 0.645 | 16.4 | 0.786 | 20.0 |
| B | 0.712 | 18.1 | 0.844 | 21.4 | 0.972 | 24.7 |
| C | 0.297 | 7.5 | 0.388 | 9.9 | 0.447 | 11.4 |



## REED BENEFITS

- Available as 4.5-30 VDC model for simple interfacing to sequencers and programmable controllers.
- Can be used to directly drive some types of relays or valve solenoids within the switch specifications stated.

| SPECIFICATIONS | $67902 \& 67922$ |
| :--- | :---: |
| OPERATING PRINCIPLE | Magnetic Reed |
| ACTUATED BY | Piston Magnet |
| INPUT VOLTAGE | $4.5-30$ VDC |
| OUTPUT TYPE | Contact Cosure |
| CURRENT RATING | 50 mA Max. |
| OONTACT RESISTANCE | .115 Ohm Max. |
| ENVRONMENTAL | IP67 |
| OPERATING TEMP. | $-20^{\circ}$ to $85^{\circ} \mathrm{C}$ |



MAGNET FOR COMPETITOR'S REED AND SOLID STATE SWITCHES

The Series SJP can be used as an exact drop-in replacement for a competitor's commercially available rail slide. If the Series SJP is being used to replace the competitor's slide, and you wish to continue using their switches, the MA option must be specified. For additional information and switch compatibility, contact your local PHD distributor or PHD customer service.

| PART NO. | DESCRIPTION |
| :---: | :--- |
| 67902-1-02 | NPN (Sink) or PNP (Source) DC Reed, 2 m cable |
| 67902-1-05 | NPN (Sink) or PNP (Source) DC Reed, 5 m cable |
| $67903-1-02$ | NPN (Sink) DC Solid State, 2 m cable |
| $67903-1-05$ | NPN (Sink) DC Solid State, 5 m cable |
| 67904-1-02 | PNP (Source) DC Solid State, 2 m cable |
| 67904-1-05 | PNP (Source) DC Solid State, 5 m cable |
| $67922-1$ | NPN (Sink) or PNP (Source) DCReed, Quick Connect |
| $67923-1$ | NPN (Sink) DC Solid State, Quick Connect |
| 67924-1 | PNP (Source) DC Solid State, Quick Connect |
| $63549-02$ | 2 m Cordset with Quick Connect |
| $63549-05$ | 5 m Cordset with Quick Connect |

## SOLID STATE BENEFITS

- Solid state switches afford long life. Constant amplitude output allows use with most digital logic systems.
- Switch circuitry protects against voltage surges and other electrical anomalies associated with operating systems.
- Excellent switch hysteresis characteristics and symmetry.
- Offered in 4.5-30 VDC current sinking and current sourcing versions for simple interfacing to electronic system controllers.

| SPECIFICATIONS | 67903 \& $67923 \quad 67904$ \& 67924 |
| :---: | :---: |
| OPERATING PRINCIPLE | Solid State |
| ACTUATED BY | Piston Magnet |
| INPUT VOLTAGE | 4.5-30 VDC |
| OUTPUT TYPE | NPN (Sink) PNP (Source) |
| QURRENT RATING | 50 mA Max |
| VOLTAGE DROP | . 5 VDC |
| SWITCHBURDEN | 10 mA . Max. |
| ENVIRONMENTAL | IP67 |
| OPERATINGTEMP. | $-20^{\circ}$ to $85^{\circ} \mathrm{C}$ |

MALE QUICK CONNECT DETAIL


METRIC INFORMATIONSHOWN IN[ ]

63549-xx CORDSET WITH FEMALE QUICK CONNECT

(800) 624-8511

## TO ORDER SPECIFY:

Product, Series, Bearing Type, Carriage
Style, Design No., Size, Travel, Travel
Adjustment, Shock Absorber Installed, and Miscellaneous Options.


SHOCK ABSORBER INSTAUED OPTION
NE1x - Shock absorber installed on extend, position 1
NE2x - Shock absorber installed on extend, position 2
NRx - Shock absorber installed on retract
" $x$ " indicates shock absorber dampening constant (2 or 3) which must be specified by the customer.

## BENEFITS: SERIES STP SLIDES WITH RAIL BEARING

## BENEFITS

- Series STP Slides provide smooth precise linear motion with high accuracy at twice the thrust of a single bore cylinder.
- Available in five bore sizes with a choice of three travel lengths to fit a wide range of applications. Optional travel adjustments allow precise adjustment of travel.
- Available in both imperial and metric versions for applications in worldwide markets.
- Standard internal and external shock pads eliminate metal to metal contact reducing noise and end-of-travel impact forces.
- Fully integrated shock absorbers and travel adjustments with shock pads allow easy adjustment from back of slide while not increasing overall package width.
- Shock absorbers and travel adjustments on retract eliminate pitch and yaw moments usually associated with externally mounted shocks and travel adjustments.
- Series STP units have increased stopping capacity and minimal deflection when travel adjustment and/or shock absorbers are used in both positions.
- Slide housing incorporates twin switch slots for flush installation of PHD's new Series 6790 reed and solid state switches.
- Consult PHD for 4 mm and 8 mm proximity switch ready units.
- All units have customer mounting and dowel holes in the housing, carriage, and tool plate.
- Modular mounting kits allow quick connect of same size Series STP Slides without the need for transition plates. See page 5A-34 for details.
- Standard stainless steel fasteners eliminate the need for costly corrosion resistant options. Combining this with -Q6 shaft option provides a completely corrosion resistant unit.


|  | BORE SIZE |
| :--- | :---: |
| SPECIFICATIONS | $\mathbf{0 8} \quad$ 12, 16, 20, \& 25 |
| POWER SOURCE | Two cylinders built into the Slide Body |
| WORKING PRESSURE | 20 psi min -150 psi max at zero load |
| TEMPERATURERANGE | $-20^{\circ}$ to $+180^{\circ} \mathrm{F}\left[-29^{\circ}\right.$ to $\left.82^{\circ} \mathrm{C}\right]$ |
| LUBRICATION | Permanent for Non-Lubricated or Lubricated Air |
| GUIDE SHAFTS | Stainless Steel Chrome Plated Steel |
| BEARINGS | Stainless Steel Ground Rail System with Recirculating Ball Bearings |
| CARRIAGE | Anodized Aluminum Alloy |
| TOOL PLATE | Anodized Aluminum Alloy |
| BODY | Anodized Aluminum Alloy |





NOTES
1）ALL DIMENSIONS ARE SYMMEIRICAL ABOUT CENIERLINEOF DOWE HO ES UNIESS OTHERWISESPECIAED
2）MEIRIC INFORMATION SHOWNIN［ ］
3）RUNNING PARALLE ISM TODATUM A IS ． 002 in $[.05 \mathrm{~mm}]$ AT 2 in ［ 50 mm ］OF TRAVE．
4）$\perp=$ PERPENDICULARITY TOLERANCE，THIS DEIERMINES HOW FAR 円ROM $90^{\circ}$ THAT THE INDICATED ÆATURES CAN BE TOTHE INDICATED DATUM ÆATURES．THIS SURFACEIS ORIENIED（ $90^{\circ}$ ） TO THE INDICATED DATUM SURFACES WITHIN A TO－囚RANCE BAND OF． 005 ［．13］
5）$/ /=$ PARALLEISM TOLERANCE THIS TOLERANCE DEIERMINES HOW PARALLE（ $180^{\circ}$ ）THAT THE INDICATED 氏ATURES CAN BE TOTHE INDICATEDATM TATURES TIESURFACEISPARAL （ $180^{\circ}$ ）TOTHEINDICATED DATUM SURFAOESWITHINATO－RANOE BAND OF． 005 ［．13］


MEIRIC INFORMATION SHOWN IN [ ].

## ENGINEERING DATA: SERIES STP SLIDES WITH RAIL BEARING

## PRESSURE RATINGS

All Series STP Slides have an operating pressure range of 20 psi minimum to 150 psi maximum [ 1.4 to 10 bar ].

## BREAKAWAY

Units have less than 20 psi [1.4 bar] breakaway with zero load.

## OPERATING TEMPERATURE

Series STP Slides are designed for use in temperatures between $20^{\circ}$ to $180^{\circ} \mathrm{F}\left[-6^{\circ}\right.$ to $82^{\circ} \mathrm{C}$. For temperatures outside this range, consult PHD.

## SEALS

Series STP Slides utilize urethane and Nitrile seals which are compatible with standard paraffin-based lubrication oils used for pneumatic cylinders. For compatibility with other fluids, consult PHD.

## LUBRICATION

All units are pre-lubricated at the factory for service under normal operating conditions. Slides are designed and tested with non-lubricated air. However, the use of lubricated air will extend life.

## OPERATING SLIDE VELOCITY

For sizes 08 and 12 , slide velocity is $36 \mathrm{in} / \mathrm{sec}$ [ $914 \mathrm{~mm} / \mathrm{sec}$ ] for extend and $24 \mathrm{in} / \mathrm{sec}$ [ $610 \mathrm{~mm} / \mathrm{sec}$ ] on retract. For sizes 16,20 , and 25 , slide velocity is $30 \mathrm{in} / \mathrm{sec}$ [ $962 \mathrm{~mm} / \mathrm{sec}$ ] for extend and 24 $\mathrm{in} / \mathrm{sec}$ [ $610 \mathrm{~mm} / \mathrm{sec}$ ] on retract. These values are based on an unloaded slide at 87 psi [6 bar] operating pressure.

## MATERIAL SPECIFICATIONS

The slide housing, tool plate, and carriage are anodized aluminum alloy. Linear rails and bearings are hardened and ground stainless steel. On standard sizes 12, 16, 20, and 25 slides, the shafts are hard chrome plated steel. Size 08 slides have stainless steel shafts. The corrosion resistant option on sizes 12, 16, 20, and 25 provides hard chrome plated stainless steel shafts.

## MAINTENANCE

In common with most PHD products, these slides are fully field repairable. Repair kits and main structural components are available as needed for extended service life.

## TOTAL TRAVEL LENGTH

Tolerance on specified minimum travel length is $+.098 /-.000$ [ $+2.5 \mathrm{~mm} /-0 \mathrm{~mm}$ ].

|  | MINIMUM <br> SIZE |  |
| :---: | :---: | :---: |
| TRAVEL |  |  |
|  | mm |  |
| 08 | 1 | 25 |
|  | 2 | 51 |
|  | 3 | 76 |
| 12 | 1 | 25 |
|  | 2.5 | 64 |
|  | 4 | 102 |
| 16 | $1-1 / 2$ | 38 |
|  | 3 | 76 |
|  | 5 | 127 |
| 20 | 2 | 51 |
|  | 4 | 102 |
|  | 6 | 152 |
| 25 | 2 | 51 |
|  | 4 | 102 |
|  | 6 | 152 |

UNIT WEGHT

| SIZE | TRAVEL |  | BASE WEIGHT |  | OPTION ADDERS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | -AR | -NRx |  | -AEx OR NEx |  |
|  | in | mm |  |  | lb | kg | lb | kg | lb | kg | lb | kg |
| 08 | 1 | 25 | 0.55 | 0.25 | 0.03 | 0.014 | 0.11 | 0.05 | 0.06 | 0.03 |
|  | 2 | 50 | 0.81 | 0.37 | 0.04 | 0.018 | 0.11 | 0.05 |  |  |
|  | 3 | 75 | 1.01 | 0.46 | 0.05 | 0.023 | 0.11 | 0.05 |  |  |
| 12 | 1 | 25 | 1.12 | 0.51 | 0.10 | 0.05 | 0.09 | 0.04 | 0.09 | 0.04 |
|  | 2-1/2 | 60 | 1.71 | 0.78 | 0.15 | 0.07 | 0.178 | 0.08 |  |  |
|  | 4 | 100 | 2.26 | 1.03 | 0.20 | 0.09 | 0.298 | 0.14 |  |  |
| 16 | 1-1/2 | 38 | 2.10 | 0.95 | 0.22 | 0.10 | 0.19 | 0.09 | 0.13 | 0.06 |
|  | 3 | 75 | 2.68 | 1.22 | 0.29 | 0.13 | 0.26 | 0.12 |  |  |
|  | 5 | 125 | 3.63 | 1.65 | 0.40 | 0.18 | 0.37 | 0.17 |  |  |
| 20 | 2 | 50 | 3.62 | 1.64 | 0.65 | 0.30 | 0.32 | 0.15 | 0.27 | 0.12 |
|  | 4 | 100 | 5.24 | 2.38 | 0.85 | 0.39 | 0.512 | 0.23 |  |  |
|  | 6 | 150 | 6.64 | 3.01 | 1.03 | 0.47 | 0.687 | 0.31 |  |  |
| 25 | 2 | 50 | 5.46 | 2.48 | 0.57 | 0.26 | 0.42 | 0.19 | 0.29 | 0.13 |
|  | 4 | 100 | 7.55 | 3.43 | 0.87 | 0.39 | 0.73 | 0.33 |  |  |
|  | 6 | 150 | 9.55 | 4.34 | 1.16 | 0.53 | 1.02 | 0.46 |  |  |

## ENGINEERING DATA: SERIES STP SLIDES WITH RAIL BEARING

## SLIDE SELECTION

There are three major factors to consider when selecting a slide: thrust capacity, allowable static and dynamic moment capacity, and table deflection (as either pitch, yaw, or roll).

## 1 THRUST CAPACITY

Use the effective piston area (seethrust specifications) of the slide to determine if thrust is sufficient for the applied load.

2 STATIC AND DYNAMIC MOMENT CAPACITY
The maximum static moments for all units are listed in the static moment chart below and must not be exceeded. The maximum allowable dynamic moment is equal to $1 / 10$ the maximum static moment in consideration of the load inertia. Calculate static and dynamic moments of the system using the following equations and diagrams:

Mp (Pitch) $=(\mathrm{Ah}+\mathrm{OG}) \times$ LOAD or $(\mathrm{Av}+\mathrm{OG}) \times$ LOAD
My (Yaw) $=(\mathrm{Ah}+\mathrm{OG}) \times$ LOAD or OG $\times$ LOAD
$\mathrm{Mr}($ Roll $)=(\mathrm{Av}+\mathrm{OG}) \times$ LOAD or $\mathrm{CG} \times$ LOAD

THRUST SPECIFICATIONS

| SIZE | SHAFT DIAMETER |  | BORE DIAMETER |  | $\begin{aligned} & \text { SHAFT } \\ & \text { DIRECTION } \end{aligned}$ | EFFECTIVE PISTON AREA |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08 | 0.157 | 4 | 0.315 | 8 | EXITND | 0.16 | 101 |
|  |  |  |  |  | REIRACT | 0.12 | 75 |
| 12 | 0.236 | 6 | 0.475 | 12 | EXTEND | 0.35 | 229 |
|  |  |  |  |  | REIRACT | 0.27 | 172 |
| 16 | 0.315 | 8 | 0.630 | 16 | EXTEND | 0.62 | 402 |
|  |  |  |  |  | REIRACT | 0.47 | 302 |
| 20 | 0.394 | 10 | 0.787 | 20 | EXIEND | 0.97 | 628 |
|  |  |  |  |  | REIRACT | 0.73 | 470 |
| 25 | 0.472 | 12 | 0.984 | 25 | EXTEND | 1.52 | 982 |
|  |  |  |  |  | REIRACT | 1.17 | 756 |


| CYLINDER THRUST CALCULATION |  |  |  |
| :---: | :---: | :---: | :---: |
|  | IMPERIAL | METRIC |  |
|  | $\mathrm{F}=\mathrm{P} \times \mathrm{A}$ | $\mathrm{F}=0.1 \times \mathrm{P} \times \mathrm{A}$ |  |
| $\mathrm{F}=$ Cylinder Force | lb | N |  |
| $\mathrm{P}=$ Operating Pressure | psi | bar |  |
| $\mathrm{A}=$ Effective Area | $\mathrm{in}^{2}$ | $\mathrm{~mm}^{2}$ |  |

(continued on next six pages)
STATIC MOMENT CHART

| SIZE | TRAVEL |  | MAX PITCH MOMENT (Mp) |  | MAX YAW MOMENT (My) |  | MAX ROLL MOMENT (Mr) |  | MOMENT ARM Ah |  | MOMENT ARM Av |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | mm | in-lb | Nm | in-lb | Nm | in-lb | Nm | in | mm | in | mm |
| 08 | 1 | 25 | 42.4 | 4.8 | 42.4 | 4.8 | 67 | 7.6 | 2.442 | 62.0 |  |  |
|  | 2 | 50 | 168 | 19.0 | 141 | 15.9 | 76 | 8.6 | 3.830 | 97.3 | 0.335 | 8.5 |
|  | 3 | 75 | 227 | 25.6 | 190 | 21.5 | 76 | 8.6 | 4.914 | 124.8 |  |  |
| 12 | 1 | 25 | 146 | 16.5 | 124 | 14.0 | 127 | 14.4 | 2.717 | 69.0 |  |  |
|  | 2-1/2 | 60 | 351 | 39.7 | 298 | 33.7 | 181 | 20.5 | 4.557 | 115.7 | 0.453 | 11.5 |
|  | 4 | 100 | 474 | 53.6 | 403 | 45.5 | 181 | 20.5 | 6.308 | 160.2 |  |  |
| 16 | 1-1/2 | 38 | 238 | 26.9 | 200 | 22.6 | 271 | 30.6 | 3.711 | 94.3 |  |  |
|  | 3 | 75 | 488 | 55.1 | 410 | 46.3 | 271 | 30.6 | 5.049 | 128.2 | 0.492 | 12.5 |
|  | 5 | 125 | 664 | 75.0 | 558 | 63.0 | 271 | 30.6 | 7.292 | 185.2 |  |  |
| 20 | 2 | 50 | 497 | 56.2 | 418 | 47.2 | 550 | 62.2 | 4.286 | 108.9 |  |  |
|  | 4 | 100 | 1290 | 145.8 | 1084 | 122.5 | 733 | 82.9 | 6.721 | 170.7 | 0.61 | 15.5 |
|  | 6 | 150 | 1772 | 200.2 | 1488 | 168.1 | 733 | 82.9 | 9.034 | 229.5 |  |  |
| 25 | 2 | 50 | 796 | 89.9 | 668 | 75.5 | 991 | 112 | 4.488 | 114.0 |  |  |
|  | 4 | 100 | 1592 | 179.9 | 1338 | 151.2 | 991 | 112 | 6.811 | 173.0 | 0.748 | 19.0 |
|  | 6 | 150 | 2112 | 238.6 | 1774 | 200.4 | 991 | 112 | 9.194 | 233.5 |  |  |

For more detail in determining table deflection; se page 5A-22 for pitch, page $5 \mathrm{~A}-24$ for yaw, and page $5 \mathrm{~A}-26$ for roll.


## ENGINEERING DATA: SERIES STP SLIDES WITH RAIL BEARING

3 STATIC DEFLECTIONS IN PITCH
The graphs on this page show table pitch deflection due to static moment loads applied at distance Ah from bearing center while the unit is extended.


| SIZE |  |  | TRAVEL |  |
| :---: | :---: | :---: | :---: | :---: |
|  | mm | MOMENT ARM |  |  |
|  | mm |  |  |  |
|  | 1 | 25 | 2.442 | 62.0 |
|  | 2 | 50 | 3.830 | 97.3 |
|  | 3 | 75 | 4.914 | 124.8 |
| 12 | 1 | 25 | 2.717 | 69.0 |
|  | $2-1 / 2$ | 60 | 4.557 | 115.7 |
|  | 4 | 100 | 6.308 | 160.2 |
| 16 | $1-1 / 2$ | 38 | 3.711 | 94.3 |
|  | 3 | 75 | 5.049 | 128.2 |
|  | 5 | 125 | 7.292 | 185.2 |
| 20 | 2 | 50 | 4.286 | 108.9 |
|  | 4 | 100 | 6.721 | 170.7 |
|  | 6 | 150 | 9.034 | 229.5 |
| 25 | 2 | 50 | 4.488 | 114.0 |
|  | 4 | 100 | 6.811 | 173.0 |
|  | 6 | 150 | 9.194 | 233.5 |

All tabulated and plotted values are typical and were determined empirically.






## ENGINEERING DATA: sERIES STP SLIDES WITH RAIL BEARING

## IMPERIAL EXAMPLE:

Determine the pitch deflection of a STPD125 x 6 slide at the center of gravity (OG) of a 10 lb load weight attached to the tool plate. The OG of the load is 2" further from the tool plate.

Calculate the moment of the application and the equivalent load at distance Ah.

$$
\begin{aligned}
\text { Mp } & =\text { Load } \times(\text { Ah distance }+ \text { OGdistance }) \\
& =10 \times(9.194+2)=112 \text { in-lb }
\end{aligned}
$$

Equivalent load $=(\mathrm{Mp} / \mathrm{Ah})=112 / 9.194=12 \mathrm{lb}$
Read the graph for a 12 lb load, deflection is approximately .003 ".

$$
\begin{aligned}
\text { Deflection Ratio } & =\text { Deflection at tool plate } / \text { Ah distance } \\
& =.003 / 9.194=3.26 \times 10^{-4}
\end{aligned}
$$

Deflection at load $=$ Deflection Ratio $\times(\mathrm{Ah}+\mathrm{OG})$

$$
=3.26 \times 10^{-4} \times(9.194+2)=.0037^{\prime \prime}
$$

## METRIC EXAMPLE:

Determine the pitch deflection of a STPD525 x 150 slide at the center of gravity (OG) of a 45 N load weight attached to the tool plate. The OG of the load is 50 mm further from the tool plate.

Calculate the moment of the application and the equivalent load at distance Ah.

Mp = Load x (Ah distance + OG distance) / 1000

$$
=45 \times(233.5+50) / 1000=12.76 \mathrm{Nm}
$$

Equivalent load $=(M p / A h) \times 1000=12.76 / 233.5 \times 1000=55 N$
Read the graph for a 55 N load, deflection is approximately .08 mm .
Deflection Ratio $=$ Deflection at tool plate / Ah distance

$$
=.08 / 233.5=3.4 \times 10^{-4}
$$

Deflection at load $=$ Deflection Ratio $\times(\mathrm{Ah}+\mathrm{OG})$

$$
=3.4 \times 10^{-4} \times(233.5+50)=.096 \mathrm{~mm}
$$

## ENGINEERING DATA: SERIES STP SLIDES WITH RAIL BEARING

3 STATIC DEFLECTIONS IN YAW
The graph below shows table yaw deflection due to static moment loads applied at distance Ah from bearing center with the unit extended.


| SIZE | TRAVEL <br> in |  | moMENT ARM <br> ma |  |
| :---: | :---: | :---: | :---: | :---: |
|  | mm |  |  |  |
|  | 1 | 25 | 2.442 | 62.0 |
|  | 2 | 50 | 3.830 | 97.3 |
|  | 3 | 75 | 4.914 | 124.8 |
| 12 | 1 | 25 | 2.717 | 69.0 |
|  | $2-1 / 2$ | 60 | 4.557 | 115.7 |
|  | 4 | 100 | 6.308 | 160.2 |
| 16 | $1-1 / 2$ | 38 | 3.711 | 94.3 |
|  | 3 | 75 | 5.049 | 128.2 |
|  | 5 | 125 | 7.292 | 185.2 |
| 20 | 2 | 50 | 4.286 | 108.9 |
|  | 4 | 100 | 6.721 | 170.7 |
|  | 6 | 150 | 9.034 | 229.5 |
| 25 | 2 | 50 | 4.488 | 114.0 |
|  | 4 | 100 | 6.811 | 173.0 |
|  | 6 | 150 | 9.194 | 233.5 |

All tabulated and plotted values are typical and were determined empirically.






## ENGINEERING DATA: SERIES STP SLIDES WITH RAIL BEARING

## IMPERIAL EXAMPLE:

Determine the yaw deflection of a STPD125 $\times 6$ slide at the center of gravity (OG) of a 10 lb load weight attached to the tool plate. The OG of the load is 2" further from the tool plate.

Calculate the moment of the application and the equivalent load at distance Ah.

$$
\begin{aligned}
\text { Mp } & =\text { Load } \times(\text { Ah distance }+ \text { OG distance }) \\
& =10 \times(9.194+2)=112 \text { in-lb }
\end{aligned}
$$

Equivalent load $=(\mathrm{My} / \mathrm{Ah})=112 / 9.194=12 \mathrm{lb}$
Read the graph for a 12 lb load, deflection is approximately $.0015^{\prime \prime}$.
Deflection Ratio $=$ Deflection at tool plate $/$ Ah distance

$$
=.0015 / 9.194=1.63 \times 10^{-4}
$$

Deflection at load $=$ Deflection Ratio $\times(A h+O G)$

$$
=1.63 \times 10^{-4} \times(9.194+2)=.0018 \text { " }
$$

## METRIC EXAMPLE:

Determine the yaw deflection of a STPD525 x 150 slide at the center of gravity (OG) of a 45 N load weight attached to the tool plate. The OG of the load is 50 mm further from the tool plate.

Calculate the moment of the application and the equivalent load at distance Ah.

My = Load x (Ah distance + OG distance) / 1000

$$
=45 \times(233.5+50) / 1000=12.76 \mathrm{Nm}
$$

Equivalent load $=(M y / A h) \times 1000=12.76 / 233.5 \times 1000=55 N$
Read the graph for a 55 N load, deflection is approximately .04 mm .
Deflection Ratio $=$ Deflection at tool plate $/$ Ah distance

$$
=.04 / 233.5=1.71 \times 10^{-4}
$$

Deflection at load $=$ Deflection Ratio $\times(A h+O G)$

$$
=1.71 \times 10^{-4} \times(233.5+50)=.048 \mathrm{~mm}
$$

## ENGINEERING DATA: SERIES STP SLIDES WITH RAIL BEARING

3 STATIC DEFLECTION IN ROLL
The graph on this page shows table roll deflection due to static moment loads applied at distance $L$ from the center of the bearing. Values plotted in graphs were measured at point indicated.


|  | TRAVEL in mm | DISTANCE L |  | $\begin{gathered} \text { DISTANCE } \\ \text { AR } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE |  | in | mm | in | mm |
| 08 | 1 25 <br> 2 50 <br> 3 75 | 2 | 51 | 0.827 | 21.0 |
| 12 | $\begin{array}{cc} 1 & 25 \\ 2-1 / 2 & 60 \\ 4 & 100 \end{array}$ | 2.5 | 64 | 1.042 | 26.5 |
| 16 | $\begin{array}{\|cc} \hline 1-1 / 2 & 38 \\ 3 & 75 \\ 5 & 125 \end{array}$ | 3.5 | 89 | 1.418 | 36.0 |
| 20 | 2 50 <br> 4 100 <br> 6 150 | 4.5 | 114 | 1.515 | 38.5 |
| 25 | 2 50 <br> 4 100 <br> 6 150 | 6 | 152 | 1.811 | 46.0 |

All tabulated and plotted values are typical and were determined empirically.






## ENGINEERING DATA: SERIES STP SLIDES WITH RAIL BEARING

## IMPERIAL EXAMPLE:

Determine the roll deflection of a STPD125 x 6 slide at the center of gravity (OG) of a 10 lb load weight at 4 " from the center of the slide.

Calculate the moment of the application and the equivalent load at distance L.

$$
\begin{aligned}
\mathrm{Mr} & =\text { Load } \times \text { Distance to OG of load } \\
& =10 \times 4=40 \text { in-lb }
\end{aligned}
$$

Equivalent load at $L=M r / L=40 / 6=6.66 \mathrm{lb}$
Read the graph for a 6.7 lb load, deflection is approximately .0005 ". (This is at AR distance of 1.811)

Deflection Ratio $=$ Deflection at AR / AR distance

$$
=.0005 / 1.811=2.76 \times 10^{-4}
$$

Deflection at load = Deflection Ratio $\times$ (OGdistance)

$$
=2.76 \times 10^{-4} \times 4=.0011^{\prime \prime}
$$

## METRIC EXAMPLE:

Determine the roll deflection of a STPD5 $25 \times 150$ slide at the center of gravity (OG) of a 45 N load weight at 102 mm from center of the slide.

Calculate the moment of the application and the equivalent load at distance L.
$\begin{aligned} \mathrm{Mr} & =\text { Load } \times \text { Distance to OG of load } / 1000 \\ & =45 \times 102 / 1000=4.59 \mathrm{Nm}\end{aligned}$
Equivalent load at $\mathrm{L}=(\mathrm{Mr} / \mathrm{L}) \times 1000=(4.59 / 152) \times 1000=30.2 \mathrm{~N}$
Read the graph for a 30.2 N load, deflection is approximately .013 mm . (This is at AR distance of 46 mm .)

Deflection Ratio $=$ Deflection at AR / AR distance

$$
=.013 / 46=2.82 \times 10^{-4}
$$

Deflection at load $=$ Deflection Ratio $\times$ (OGdistance)

$$
=2.82 \times 10^{-4} \times 102=.029 \mathrm{~mm}
$$

## SLIDE SIZING EXAMPLE: SERIES STP SLIDES WITH RAIL bearing

## IMPERIAL

Step 1: Determine Application Data Pick and place application as shown. Total Weight of vertical slide $=4.8 \mathrm{lb}$ Total Weight of gripper and tooling $=.6 \mathrm{lb}$ Total Weight of gripped object $=.1 \mathrm{lb}$ Operating pressure $=80 \mathrm{psi}$
Required Travel = 5"
OGDist =1"


## METRIC

Step 1: Determine Application Data Pick and place application as shown. Total Weight of vertical slide $=21.4 \mathrm{~N}$ Total Weight of gripper and tooling $=2.7 \mathrm{~N}$
Total Weight of gripped object $=.4 \mathrm{~N}$
Operating pressure $=5.5$ bar
Required Travel $=125 \mathrm{~mm}$
OGDist $=25 \mathrm{~mm}$

Step 2: Determine the Total Weight of the system and the required thrust of the slide.
Calculate the Total Weight of the system:
Weight of attached slide $=\quad 4.8$
Weight of gripper and tooling = . 6
Weight of gripped object $=\quad \frac{.1}{5.5 \mathrm{lb}}$
Total Weight $=$
Weight =
Since the application is horizontal, thrust calculation is not required at this step due to very low friction values.

Size 16 would be the minimum requirement based on the necessary travel.

Step 3: Determine static and dynamic moment capacity First check size 16 for moment capacity.
From the Static Moment Chart for Yaw moment, Maximum yaw moment (My) for a 5" travel = 558 in- lb and $\mathrm{Ah}=7.292^{\prime \prime}$
$M y=(A h+O G) \times$ LOAD (Total Weight)
My Static $=(7.292+1) \times 5.5=45.6$ in-lb, okay statically
My Dynamic $=558 / 10=55.8$ in-lb, okay dynamically
Since Dynamic moment of the system is less than 55.8 , the size 16 can be used.

Step 4: Determine the amount of Deflection
From the yaw deflection graphs, determine the amount of deflection at the tool plate by using the Total Weight calculated above and finding the crossing point for a size $16 \times 5$.
Approximately .004 of deflection at the tool plate for this application.
Note: Dynamic forces from the attached slide and gripper can cause higher deflections than the value just calculated depending on deceleration methods.
Step 5: Calculate Stopping Capacity - see page 5A-35

Step 2: Determine the Total Weight of the system and the required thrust of the slide.

Calculate the Total Weight of the system:
Weight of attached slide $=\quad 21.4$
Weight of gripper and tooling $=2.7$
Weight of gripped object $=\quad \frac{.4}{24.5 \mathrm{~N}}$
Total Weight $=$
Since the application is horizontal, thrust calculation is not required at this step due to very low friction values.
Size 16 would be the minimum requirement based on the necessary travel.

Step 3: Determine static and dynamic moment capacity First check size 16 for moment capacity.

From the Static Moment Chart for Yaw moment, Maximum yaw moment (My) for a 125 mm travel $=63 \mathrm{Nm}$ and $\mathrm{Ah}=185.2 \mathrm{~mm}$
$M y=(A h+O G) \times$ LOAD (Total Weight)
My Static $=(.1852+.025) \times 24.5=5.1 \mathrm{Nm}$, okay statically
My Dynamic $=63 / 10=6.3 \mathrm{Nm}$, okay dynamically
Since Dynamic moment of the system is less than 6.3, the size 16 can be used.

Step 4: Determine the amount of Deflection
From the yaw deflection graphs, determine the amount of deflection at the tool plate by using the Total Weight calculated above and finding the crossing point for a size $16 \times 125$.

Approximately .10 mm of deflection at the tool plate for this application.
Note: Dynamic forces from the attached slide and gripper can cause higher deflections than the value just calculated depending on deceleration methods.

Step 5: Calculate Stopping Capacity - see page 5A-35

## OPTIONS: SERIES STP SLIDES WITH RAIL BEARING

## AE1 <br> TRAVEL ADJUSTMENT AND SHOCK PAD ON EXTEND IN POSITION 1

This option provides travel adjustment with a shock pad on extend in position 1. Shock pads provide excellent noise reduction and energy absorption capability. Travel on extend can be reduced by a maximum of ' $A$ ' shown in the table below. Adjust travel adjustment screw to the required position using ' $G$ ' hex wrench and lock into place using ' $F$ hex wrench. Refer to page 5A-35 for stopping capacity of the shock pad.

TRAVEL ADJUSTMENT AND SHOCK PAD ON EXTEND IN POSITION 2

This option provides travel adjustment with a shock pad on extend in position 2. Shock pads provide excellent noise reduction and energy absorption capability. By using -AE1 and -AE2 options together, yaw moments are greatly reduced and may eliminate the need for a shock absorber. Travel on extend can be reduced by a maximum of ' $A$ ' shown in the table below. Adjust travel adjustment screw to the required position using ' $G$ hex wrench and lock into place using ' $F$ hex wrench. Refer to page 5A-35 for stopping capacity of the shock pad.

|  | TRAVEL |  | A |  | B |  | C |  | D |  | E |  | $\begin{gathered} \hline F \\ \text { HEX } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{G} \\ \mathrm{HEX} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |  |  |
| 08 | 1 | 25 | . 650 | 16.5 | 2.953 | 75.0 | . 591 | 15.0 | . 752 | 19.1 | 0.74 | 18.9 | 2 mm | 3 mm |
|  | 2 | 50 | . 827 | 21.0 | 3.779 | 96.0 | - | - |  |  |  |  |  |  |
|  | 3 | 75 | . 827 | 21.0 | 4.783 | 121.5 | - | - |  |  |  |  |  |  |
| 12 | 1 | 25 | . 749 | 19.0 | 2.755 | 70.0 | . 120 | 3.0 | 1.022 | 26.0 | 0.96 | 24.3 | 2.5 mm | 3 mm |
|  | 2-1/2 | 60 | . 944 | 24.0 | 4.490 | 114.0 | - | - |  |  |  |  |  |  |
|  | 4 | 100 | 1.122 | 28.5 | 6.081 | 154.5 | - | - |  |  |  |  |  |  |
| 16 | 1-1/2 | 38 | . 945 | 24.0 | 3.662 | 93.0 | . 039 | 1.0 | 1.181 | 30.0 | 1.260 | 32 | 2.5 mm | 5 mm |
|  | 3 | 75 | 1.122 | 28.5 | 4.981 | 126.5 | - | - |  |  |  |  |  |  |
|  | 5 | 125 | 1.102 | 28.0 | 6.989 | 177.5 | - | - |  |  |  |  |  |  |
| 20 | 2 | 50 | 1.281 | 32.5 | 4.152 | 105.5 | - | - | 1.447 | 36.8 | 1.42 | 36 | 2.5 mm | 6 mm |
|  | 4 | 100 | 1.654 | 42.0 | 6.576 | 167.0 | - | - |  |  |  |  |  |  |
|  | 6 | 150 | 1.299 | 33.0 | 8.896 | 226.0 | - | - |  |  |  |  |  |  |
| 25 | 2 | 50 | 1.437 | 36.5 | 4.487 | 114.0 | . 354 | 9.0 | 1.810 | 46.0 | 1.71 | 43.5 | 3 mm | 6 mm |
|  | 4 | 100 | 1.181 | 30.0 | 6.732 | 171.0 | - | - |  |  |  |  |  |  |
|  | 6 | 150 | 1.122 | 28.5 | 8.800 | 223.5 | - | - |  |  |  |  |  |  |



## AR <br> TRAVEL ADJUSTMENT AND SHOCK PAD ON RETRACT

This option provides travel adjustment with a shock pad on retract. Shock pads provide excellent noise reduction and energy absorption capability. Travel on retract can be reduced by a maximum of ' $A$ ' shown in the table below. Adjust travel adjustment screw to the required position using ' $B$ ' hex wrench and lock into place using ' $C$ hex wrench. Refer to page 5A-35 for stopping capacity of the shock pad.

|  | A |  | B | C |
| :---: | :---: | :---: | :---: | :---: |
| SIZE | in | mm | HEX | HEX |
| 08 | .512 | 13.0 | 2 mm | 3 mm |
| 12 | .669 | 17.0 | 4 mm | 5 mm |
| 16 | .984 | 25.0 | 5 mm | 6 mm |
| 20 | 1.063 | 27.0 | 6 mm | 8 mm |
| 25 | 1.063 | 27.0 | 6 mm | 10 mm |



All dimensions are reference only unless specifically toleranced.

## OPTIONS: SERIES STP SLIDES WITH RAIL BEARING

This option provides a compromise fit between clearance and interference. Transitional fits are used where accuracy of location is important, but a small amount of clearance is permissible.


PRECISION FIT DOWEL PIN HOLES

This option provides a H7 tolerance precision fit with dowel pins. Precision fits are used where accuracy of location is of prime importance and for parts requiring rigidity and alignment.


| Ø R DOWEL HOLE | TOLERANCE |  |  |
| :---: | :---: | :---: | :---: |
|  | STANDARD | J3 OPTION | J8 OPTION |
| 3 mm | +.0004/-. 0009 | +.0013/+. 0003 | +.0004/-.0000 |
|  | [+.010/.-024] | [ $+.033 /+.008$ ] | [ $+.010 /-.000]$ |
| 4 mm | +.0004/-.0009 | +.0015/+.0005] | +.0005/-.0000 |
|  | [+.010/.-024] | [ $+.033 /+.008$ ] | [ $+.010 /-.000]$ |
| 5 mm | +.0004/-.0009 | +.0015/+.0004] | +.0005/-.0000 |
|  | [+.010/.-024] | [ $+.038 /+.010$ ] | [+.012/-000] |
| 6 mm | +.0004/-.0009 | +.0015/+.0005] | +.0005/-.0000 |
|  | [+.010/..024] | [+.038/+.013] | [ $+.012 /-.000$ ] |




DIAMETRAL ZONE


BILATERAL ZONE

## OPTIONS: SERIES STP SLIDES WITH RAIL BEARING

M MAGNET FOR PHD SERIES 6790 MINIATURE REED AND SOLID STATE SWITCHES

This option equips the unit with a magnetic piston for use with PHD's Series 6790 Switch. The switch housing is completely contained by the slide housing and provides a very compact switch design. The switches mount easily into two small grooves located on the side of the slide housing and are locked into place with a set screw.

## REED BENEFITS

- Available as 4.5-30 VDC model for simple interfacing to sequencers and programmable controllers.
- Can be used to directly drive some types of relays or valve solenoids within the switch specifications stated.

| SPECIFICATIONS | $67902 \& 67922$ |
| :--- | :---: |
| OPERATING PRINCIPLE | Magnetic Reed |
| ACTUATED BY | Piston Magnet |
| INPUT VOTAGE | $4.5-30$ VDC |
| OUTPUT TYPE | Contact Cosure |
| CURRENT RATING | 50 mA Max. |
| CONTACT RESISTANCE | .115 Ohm Max. |
| QNVIRONMENTAL | IP67 |
| OPERATING TEMP. | $-20^{\circ}$ to $85^{\circ} \mathrm{C}$ |


| SIZE | REPEATABILITY | HYSTERESIS <br> MAXIMUM | BINIMUM/MAXIMUM |  |
| :---: | :---: | :---: | :---: | :---: |
| MINIDTH |  |  |  |  |
| 08 | $\pm .005[ \pm .13]$ | $.060[1.5]$ | $.360 / .690$ | $[9.1 / 17.5]$ |
| 12 | $\pm .005[ \pm .13]$ | $.080[2.0]$ | $.230 / .340$ | $[5.8 / 8.6]$ |
| 16 | $\pm .005[ \pm .13]$ | $.075[1.9]$ | $.340 / .440$ | $[8.6 / 11.2]$ |
| 20 | $\pm .005[ \pm .13]$ | $.085[2.2]$ | $.130 / .360$ | $[3.3 / 9.1]$ |
| 25 | $\pm .004[ \pm .10]$ | $.070[1.8]$ | $.300 / .425$ | $[7.6 / 10.8]$ |



## PART NO.

67902-1-02
67902-1-05 NPN (Sink) or PNP (Source) DC Reed, 5 m cable
67903-1-02 NPN (Sink) DC Solid State, 2 m cable
67903-1-05 NPN (Sink) DC Solid State, 5 m cable
67904-1-02 PNP (Source) DC Solid State, 2 m cable
67904-1-05 PNP (Source) DC Solid State, 5 m cable
67922-1 NPN (Sink) or PNP (Source) DC Reed, Quick Connect
67923-1 NPN (Sink) DC Solid State, Quick Connect
67924-1 PNP (Source) DC Solid State, Quick Connect
63549-02 2 m Cordset with Quick Connect
63549-05 5 m Cordset with Quick Connect


## SOLID STATE BENEFITS

- Solid state switches afford long life. Constant amplitude output allows use with most digital logic systems.
- Switch circuitry protects against voltage surges and other electrical anomalies associated with operating systems.
- Excellent switch hysteresis characteristics and symmetry.
- Offered in 4.5-30 VDC current sinking and current sourcing versions for simple interfacing to electronic system controllers.

| SPECIFICATIONS | $\mathbf{6 7 9 0 3 ~ \& ~ 6 7 9 2 3 ~} \mathbf{6 7 9 0 4}$ \& $\mathbf{6 7 9 2 4}$ |
| :--- | :---: |
| OPRATINGPRINCIPLE | Solid State |
| ACTUATED BY | Piston Magnet |
| INPUT VOLTAGE | $4.5-30$ VDC |
| OUTPUT TYPE | PNP (Source) |
| CURRENT RATING | $50 \mathrm{~mA} . \mathrm{Max}$ |
| VOLTAGE DROP | .5 VDC |
| SWITCH BURDEN | 10 mA. Max. |
| ENVIRONMENTAL | IP67 |
| OPERATING TEMP. | $-20^{\circ}$ to $85^{\circ} \mathrm{C}$ |


| SIZE | REPEATABILITY | HYSTERESIS <br> MAXIMUM | BAND WIDTH <br> MINIMUM/MAXIMUM |  |
| :---: | :---: | :---: | :---: | :---: |
| 08 | $\pm .007[ \pm .18]$ | $.065[1.7]$ | $.320 / .580$ | $[8.1 / 14.7]$ |
| 12 | $\pm .007[ \pm .18]$ | $.095[2.4]$ | $.300 / .450$ | $[7.8 / 11.5]$ |
| 16 | $\pm .007[ \pm .18]$ | $.095[2.4]$ | $.330 / .510$ | $[8.4 / 13.0]$ |
| 20 | $\pm .005[ \pm .13]$ | $.110[2.8]$ | $.190 / .380$ | $[4.8 / 9.6]$ |
| 25 | $\pm .005[ \pm .13]$ | $.080[2.0]$ | $.320 / .470$ | $[8.1 / 11.9]$ |

MALE QUICK CONNECT DETAIL


MEIRICINFORMATIONSHOWNIN[ ]

63549-xx CORDSET WITH FEMALE QUICK CONNECT


## OPTIONS: SERIES STP SLIDES WITH RAIL BEARING

## SOLID STATE WIRING SCHEMATICS

MODEL NO. 67903-1 \& 67923-1 - NPN (SINK)
INPUT: 4.5-30 VDC
LOAD CURRENT: 50 mA . MAX. SWITCH HOUSING COLOR: BLACK
(Bi-polar LED emits a yellow light)
CABLED MODEL 67903


QUICK CONNECT MODEL 67923


MODEL NO. 67904-1 \& 67924-1 - PNP (SOURCE) INPUT: 4.5-30 VDC
LOAD CURRENT: 50 mA . MAX.
SWITCH HOUSING COLOR: BLACK
(Bi-polar LED emits a red light.)
CABLED MODEL 67904


QUICK CONNECT MODEL 67924


## REED WIRING SCHEMATICS

MODEL NO. 67902-1 \& 67922-1 - NPN (SINK) OR PNP (SOURCE)
INPUT: 4.5-30 VDC
LOAD CURRENT: 50 mA . MAX.
SWITCH HOUSING COLOR: BLACK
(LED emits a red light)
CABLED MODEL 67902 - NPN (SINK)


QUICK CONNECT MODEL 67922 - NPN (SINK)


CABLED MODEL 67902 - PNP (SOURCE)


QUICK CONNECT MODEL 67922 - PNP (SOURCE)


## NE1x SHOCK ABSORBER installed ON EXTEND IN POSITION 1

This option provides shock absorbers and travel adjustment on extend in position 1. Travel on extend can be reduced by a maximum of ' $A$ ' shown in the table below. Adjust shock absorber screw to the required position using a large screwdriver and lock into place using ' $F$ hex wrench. Refer to page 5A-36 for shock absorber selection requirements.


SHOCK ABSORBER INSTALLED ON EXTEND IN POSITION 2

This option provides shock absorbers and travel adjustment on extend in position 2. Travel on extend can be reduced by a maximum of ' $A$ ' shown in the table below. Adjust shock absorber screw to the required position using a large screwdriver and lock into place using ' $F$ hex wrench. Refer to page 5A-36 for shock absorber selection requirements.

| SIZE | TRAVEL |  | A |  | B |  | C |  | D |  | E |  | $\begin{gathered} \hline F \\ \text { HEX } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | mm | in | mm | in | mm | in | mm | in | mm |  | mm |  |
| 08 | 1 | 25 | . 650 | 16.5 | 2.953 | 75.0 | . 591 | 15.0 |  |  |  |  | 2 mm |
|  | 2 | 50 | . 827 | 21.0 | 3.779 | 96.0 | - | - | . 752 | 19.1 | 0.743 | 18.9 |  |
|  | 3 | 75 | . 827 | 21.0 | 4.783 | 121.5 | - | - |  |  |  |  |  |
| 12 | 1 | 25 | 1.064 | 27.0 | 2.755 | 70.0 | . 433 | 11.0 | 1.022 | 26.0 | 0.96 | 24.4 | 2.5 mm |
|  | 2-1/2 | 60 | 0.828 | 21.0 | 4.490 | 114.0 |  | - |  |  |  |  |  |
|  | 4 | 100 | 0.866 | 22.5 | 6.081 | 154.5 | - | - |  |  |  |  |  |
| 16 | 1-1/2 | 38 | . 945 | 24.0 | 3.662 | 93.0 | . 039 | 1.0 | 1.181 | 30.0 | 1.260 | 32 | 2.5 mm |
|  | 3 | 75 | 1.122 | 28.5 | 4.981 | 126.5 | - | - |  |  |  |  |  |
|  | 5 | 125 | 1.102 | 28.0 | 6.989 | 177.5 | - | - |  |  |  |  |  |
| 20 | 2 | 50 | 1.280 | 32.5 | 4.152 | 105.5 | - | - | 1.447 | 36.8 | 1.42 | 36 | 2.5 mm |
|  | 4 | 100 | 1.280 | 32.5 | 6.576 | 167.0 | - | - |  |  |  |  |  |
|  | 6 | 150 | 1.280 | 32.5 | 8.896 | 226.0 | - | - |  |  |  |  |  |
| 25 | 2 | 50 | 1.772 | 45.0 | 4.487 | 114.0 | . 669 | 17.0 | 1.810 | 46.0 | 1.712 | 43.5 | 3 mm |
|  | 4 | 100 | 1.516 | 38.5 | 6.732 | 171.0 | - | - |  |  |  |  |  |
|  | 6 | 150 | 1.457 | 37.0 | 8.800 | 223.5 | - | - |  |  |  |  |  |



## OPTIONS: SERIES STP SLIDES WITH RAIL BEARING

FOR SIZE 08 ONLY

## NRx <br> SHOCK ABSORBER INSTALLED ON RETRACT

This option provides shock absorbers and travel adjustment on

| A |  | D |  | E $^{\text {in }}$ |  | mm | in | mm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in $^{\text {G }}$ mm |  |  |  |  |
| .905 | 23.0 | .728 | 18.5 | 2.008 | 51.0 | .901 | 22.9 | 1.151 | retract. Travel on retract can be reduced by a maximum of ' $A$ ' shown in the table at right. Adjust travel to the required position using a large screwdriver and lock into place using 11 mm hex wrench. Refer to page 5A-36 for shock absorber selection requirements.



FOR SIZES 12, 16, 20, \& 25

This option provides shock absorbers and travel adjustment on retract. Travel on retract can be reduced by a maximum of ' $A$ ' shown in the table below. Adjust travel to the required position using 'B' hex wrench and lock into place using ' $C$ ' hex wrench. Refer to page 5A-36 for shock absorber selection requirements.

|  |  | C |  |  |
| :---: | :---: | :---: | :---: | :---: |
| MODEL | in | mm | BEX | C |
| HEX |  |  |  |  |
| STPxx12 | .512 | 13.0 | 4 mm | 5 mm |
| STPxx16 | .984 | 25.0 | 5 mm | 6 mm |
| STPxx20 | 1.063 | 27.0 | 6 mm | 8 mm |
| STPxx25 | 1.063 | 27.0 | 6 mm | 10 mm |



## Q6 CORROSION RESISTANT GUIDE SHAFTS

This option provides stainless steel guide shafts with hard chrome plating, for use in applications where the standard shaft ends may corrode.

## ACCESSORIES: SERIES STP SLIDES WITH RAIL BEARING

## MODULAR MOUNTING KITS

Modular design of the Series STP housings and tool plates allow slide units to bolt and dowel together without the need for a transition plate. See chart for slide compatibility and hardware kits required. Each kit contains 2 dowel pins and 2 SHCS to mount the units together. Series STP units can also be bolted directly together as shown. PHD recommends that a-J3 option (transitional fit) be specified with the slide ordering data to allow the units to dowel together properly.


|  |  | KIT NUMBERS |  |
| :---: | :---: | :---: | :---: |
| PRIMARY | SECONDARY | IMPERIAL | METRIC |
| STPDx08 | STPDx08 | $68125-01$ | $68125-02$ |
| STPDx12 | STPDx12 | $70770-01$ | $70770-02$ |
| STPDx16 | STPDx16 | $68053-01$ | $68053-02$ |
| STPDx20 | STPDx20 | $70870-01$ | $70870-02$ |
| STPDx25 | STPDx25 | $68043-01$ | $68043-02$ |

## STOPPING CAPACITY: SERIES STP SLIDES WITH RAIL BEARING

## STOPPING CAPACITY SELECTION

To determine stopping capacity, calculate total moving weight. From Table 1, determine slide standard moving weight, add any additional weight adders due to options and add attached payload. This will be total moving weight WTM .

Example: STPD125 x $2-A E 1-A E 2$ with 10 lb load [STPD525 x 50-AE1-AE2 with 44.5 N load]
$\mathrm{W}_{\text {тм }}=2.6 \mathrm{lb}+.29 \mathrm{lb}+.29 \mathrm{lb}+10 \mathrm{lb}=13.18 \mathrm{lb}$ [11.6 N +1.29 N +1.29 N + 44.5 N = 58.68 N ]

Using the Kinetic Energy Graphs below, plot the total moving weight against impact velocity. If the value plotted is below the curve, then shock pads are an adequate deceleration method. If it is above the curve, hydraulic shock absorbers are required.

To determine the correct hydraulic shock absorber, complete the calculations on the next page.

TABLE 1

| SIZE | TRAVEL in mm |  | STPMOVING WEIGHT |  | WEGGT ADDERS <br> -AE1, -AE2, <br> -NE1x, -NE2x |  | PISTON AREA EXTEND |  | PISTON AREA RETRACT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08 | 1 | 25 | 0.24 | 1.1 |  |  |  |  |  |  |
|  | 2 | 50 | 0.36 | 1.6 | 0.06 | 0.27 | 0.16 | 101 | 0.12 | 75 |
|  | 3 | 75 | 0.40 | 1.8 |  |  |  |  |  |  |
| 12 | 1 | 25 | 0.42 | 1.9 |  |  |  |  |  |  |
|  | 2-1/2 | 60 | 0.60 | 2.7 | 0.09 | 0.42 | 0.35 | 226 | 0.26 | 170 |
|  | 4 | 100 | 0.78 | 3.4 |  |  |  |  |  |  |
| 16 | 1-1/2 | 38 | 0.9 | 4.0 |  |  |  |  |  |  |
|  | 3 | 75 | 1.1 | 4.9 | 0.13 | 0.58 | 0.62 | 402 | 0.47 | 302 |
|  | 5 | 125 | 1.4 | 6.2 |  |  |  |  |  |  |
| 20 | 2 | 50 | 1.4 | 6.2 |  |  |  |  |  |  |
|  | 4 | 100 | 1.9 | 8.5 | 0.20 | 0.91 | 0.97 | 628 | 0.73 | 471 |
|  | 6 | 150 | 2.4 | 10.7 |  |  |  |  |  |  |
| 25 | 2 | 50 | 2.6 | 11.6 |  |  |  |  |  |  |
|  | 4 | 100 | 3.6 | 16.0 | 0.29 | 1.29 | 1.52 | 982 | 1.17 | 756 |
|  | 6 | 150 | 4.3 | 19.1 |  |  |  |  |  |  |

## MAXIMUM ALLOWABLE KINETIC ENERGY GRAPHS FOR SHOCK PADS



# SHOCK ABSORBER SELECTION GUIDE: SERIES STP 

| SIZE | $\begin{gathered} \text { PHD } \\ \text { SHOCK } \\ \text { ABSORBER } \\ \text { NO. } \\ \hline \end{gathered}$ | STROKE |  | THREAD TYPE | ET TOTAL ENERGY PER CYCLE |  | $\begin{gathered} \text { ECC } \\ \text { TOTAL ENERGY } \\ \text { PER HOUR } \end{gathered}$ |  | $\begin{gathered} \mathrm{FG}_{\mathrm{G}} \\ \text { MAX PROPELLING } \\ \text { FORCE } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | in-lb | Nm | in-lb | Nm | lb | N |
| 08 \& 12 | 68149-01-x | . 210 | . 0053 |  | M8 x1 | 20 | 2.26 | 50,000 | 5654 | 45 | 200 |
| 16 | 68015-01-x | . 240 | . 0061 | M10 $\times 1$ | 40 | 4.52 | 110,000 | 12439 | 80 | 356 |
| 20 | 70861-01-x | . 400 | . 0102 | M12 $\times 1$ | 65 | 7.35 | 250,000 | 28269 | 120 | 534 |
| 25 | 67127-01-x | . 448 | 0114 | M14 $\times 1.5$ | 135 | 15.26 | 260,000 | 29400 | 200 | 890 |

## SHOCK ABSORBER SIZING CALCULATION:

Follow the next six steps to size shock absorbers.
STEP 1: Identify the following parameters. These must be known for all energy absorption calculations. Variations or additional information may be required in some cases.
A. The total moving weight (WTM ) to be stopped. (completed from prior page)
B. The slide velocity $(\mathrm{V})$ at impact with the shock absorber.
C. Number of cycles per hour.
D. Orientation of the application's motion (i.e. horizontal or vertical application). See the next two pages.
E Operating pressure
STEP 2: Calculate the kinetic energy of the total moving weight.

$$
\mathrm{E}_{\mathrm{K}}(\mathrm{in}-\mathrm{lb})=.5 \times \frac{W_{\text {TM }}}{386} \times \mathrm{V}^{2} \quad \mathrm{E}_{\mathrm{K}}(\mathrm{Nm})=.5 \times \frac{\mathrm{W}_{\text {TM }}}{9.8} \times \mathrm{V}^{2}
$$ or

Note: WTm in kg mass may

$$
\text { be substituted for } \frac{W_{T M}}{9.8}
$$

$\mathrm{EK}_{\mathrm{K}}(\mathrm{Nm})=.5 \times \mathrm{W}_{\mathrm{T}} \mathrm{M} \times \mathrm{V}^{2}$

STEP 3: Calculate the propelling force ( $\mathrm{FD}_{\mathrm{D}}$ ) for both extend and retract. Refer to previous page for Efective Piston Areas.

Horizontal application: $\mathrm{FD}=$ Effective Piston Areax $P$ Vertical application: $F D=($ Efective Piston Areax $P) \pm W_{t M}$ + indicates working with gravity, - indicates working against gravity Note: when using $\mathrm{mm}^{2}$ and bar units, it will be necessary to multiply the Effective Piston Areax P by a factor of .1 to obtain the correct unit of measure.
Use Shock Absorber Specification Chart to verify that the selected unit has an $\mathrm{FG}_{\mathrm{G}}$ capacity greater than the value just calculated. If not, select a larger shock absorber or slide.
Calculate the work energy input ( $\mathrm{E} w=\mathrm{FD} \times \mathrm{S}$ ) using the travel of the shock absorber selected.

STEP 4: Calculate the total energy. $\mathrm{E}_{\mathrm{T}}=\mathrm{E}_{\mathrm{k}}+\mathrm{E}_{\mathrm{w}}$ Use Shock Absorber Specification Chart to verify that the selected unit has an Er capacity greater than the value just calculated. If not, select a larger shock absorber or slide.

STEP 5: Calculate the total energy that must be absorbed per hour ( $\mathrm{E}_{\mathrm{T}} \mathrm{C}$. $\mathrm{ETC}=\mathrm{Et}_{\mathrm{T}} \times \mathrm{C}$
Use Shock Absorber Specification Chart to verify that the selected unit has an ETC capacity greater than the value just calculated. If not, select a larger shock absorber or slide.

STEP 6: Determine the damping constant for the selected shock absorber. Using the appropriate Shock Absorber Performance Graph, locate the intersection point for impact velocity ( $V$ ) and total energy (ET). The area ( -2 or -3 ) that the point falls in is the correct damping constant for the application.

## SYMBOLS DEFINITIONS

C = Number of cycles per hour
= Oylinder bore diameter inch [mm]
$=$ Kinetic energy in- $\mathrm{Ib}[\mathrm{Nm}$ ]
$=$ Total energy per cycle, $\mathrm{E} \times+\mathrm{Ew}$ in- $\mathrm{lb}[\mathrm{Nm}]$
$\mathrm{EC}=$ Total energy per hour in-lb/hr [ $\mathrm{Nm} / \mathrm{hr}$ ]
Ew = Work or drive energy in-lb [Nm]
= Propelling force lb [ N ]
$=$ Max Propelling force $\mathrm{lb}[\mathrm{N}]$
= Operating pressure psi [bar]
= Stroke of shock absorber inch [m]
$=$ Impact velocity in/sec [m/sec]
$\mathrm{W}_{\mathrm{m}}=$ Total moving weight lb [ N or kg]





## SHOCK ABSORBER SELECTION GUIDE: SERIES STP

## SIZING EXAMPLE: HORIZONTAL APPLICATION



## IMPERIAL

## STEP 1: Application Data

Example: STPD125 x 6 -NEx-NRx with a 20 lb payload on extend and 1 lb on retract.
A) $\mathrm{W}_{\text {TM }}=$ Total moving weight $=$ std moving + option adder + load

Extend $=2.6 \mathrm{lb}+.29 \mathrm{lb}+20 \mathrm{lb}=22.89 \mathrm{lb}$
Retract $=2.6 \mathrm{lb}+.29 \mathrm{lb}+1 \mathrm{lb}=3.89 \mathrm{lb}$
B) Velocity at impact: $V_{E}=15 \mathrm{in} / \mathrm{sec}$ (extend), $V_{R}=20 \mathrm{in} / \mathrm{sec}$ (retract)
C) Number of cycles/hour: C=800 cycles/hr
D) Application type: Horizontal
E) Operating pressure: 80 psi

STEP 2: Calculate the kinetic energy
$\mathrm{E}_{\mathrm{K}}=.5 \times \mathrm{W}_{\mathrm{T}} \times \mathrm{V}^{2} / 386$
Extend $=.5 \times 22.89 \times 15^{2} / 386=6.67 \mathrm{in}-\mathrm{lb}$
Retract $=.5 \times 3.89 \times 20^{2} / 386=2.02 \mathrm{in}-\mathrm{lb}$
STEP 3: Calculate the propelling force and work energy $\mathrm{FD}=$ Effective Piston Area $\times$ Operating Pressure
Extend $=1.52 \times 80=121.6 \mathrm{lb}$
Retract $=1.17 \times 80=93.6 \mathrm{lb}$
Use the Shock Absorber Specification Chart to verify that the selected unit has an FG capacity greater than the value just calculated.
$\mathrm{E} v=\mathrm{FD} \times \mathrm{S}$
Extend $=121.6 \times .448=54.5 \mathrm{in}-\mathrm{lb}$
Retract $=93.6 \times .448=41.9 \mathrm{in}-\mathrm{lb}$
STEP 4: Calculate the total energy: $\mathrm{ET}_{\mathrm{T}}=\mathrm{E}_{\mathrm{k}}+\mathrm{Ew}_{\mathrm{w}}$
Extend $=6.67+54.5=61.17 \mathrm{in}-\mathrm{lb}$
Retract $=2.02+41.9=43.92 \mathrm{in}-\mathrm{lb}$
Use the Shock Absorber Specification Chart to verify that the selected unit has an Et capacity greater than the value just calculated.
STEP 5: Calculate the total energy per hour: ETC $=\mathrm{ET} \times \mathrm{C}$
Extend $=61.17 \times 800=48,397 \mathrm{in}-\mathrm{lb} / \mathrm{hr}$
Retract $=43.92 \times 800=35,136 \mathrm{in}-\mathrm{lb} / \mathrm{hr}$
Use the Shock Absorber Specification Chart to verify that the selected unit has and ETC capacity greater that the value calculated.
STEP 6: Determine the damping constant required
Using the appropriate Shock Absorber performance graph, locate the intersection point for impact velocity ( V ) and total energy ( E ). The area (-2 or -3) that the point falls in is the correct damping constant for the application.

Unit should be ordered with -NE3-NR2 options or select shock 67127-01-3 for extend and shock 67127-01-2 for retract.

## METRIC

## STEP 1: Application Data

Example: STPD525 x 150 -NEx-NRx with a 89 N payload on extend and 4.4 N on retract.
A) $\mathrm{W}_{\mathrm{T}}=$ Total moving weight $=$ std moving + option adder + load Extend $=11.6 \mathrm{~N}+1.29 \mathrm{~N}+89 \mathrm{~N}=101.89 \mathrm{~N}$
Retract $=11.6 \mathrm{~N}+1.29 \mathrm{~N}+4.4 \mathrm{~N}=17.29 \mathrm{~N}$
B) Velocity at impact: $\mathrm{V}_{\mathrm{E}}=.381 \mathrm{~m} / \mathrm{sec}$ (extend), $\mathrm{V}_{\mathrm{R}}=.51 \mathrm{~m} / \mathrm{sec}$ (retract)
C) Number of cycles/hour: $\mathrm{C}=800 \mathrm{cycles} / \mathrm{hr}$
D) Application type: Horizontal
E) Operating pressure: 5.5 bar

STEP 2: Calculate the kinetic energy
$\mathrm{E}_{\mathrm{K}}=.5 \times$ Wtм $\times \mathrm{V}^{2} / 9.8$
Extend $=.5 \times 101.89 \times .381^{2} / 9.8=.75 \mathrm{Nm}$
Retract $=.5 \times 17.29 \times .51^{2} / 9.8=.23 \mathrm{Nm}$
STEP 3: Calculate the propelling force and work energy
FD $=$ Effective Piston Area $\times$ Operating Pressure $\times .1$
Extend $=982 \times 5.5 \times .1=540 \mathrm{~N}$
Retract $=756 \times 5.5 \times .1=416 \mathrm{~N}$
Use the Shock Absorber Specification Chart to verify that the selected unit has an FG capacity greater than the value just calculated.
$\mathrm{E} w=\mathrm{FD} \times \mathrm{S}$
Extend $=540 \times .0114=6.16 \mathrm{Nm}$
Retract $=416 \times .0114=4.74 \mathrm{Nm}$
STEP 4: Calculate the total energy: $\mathrm{ET}_{\mathrm{t}}=\mathrm{Ek}+\mathrm{Ew}$
Extend $=.75+6.16=6.91 \mathrm{Nm}$
Retract $=.23+4.74=4.97 \mathrm{Nm}$
Use the Shock Absorber Specification Chart to verify that the selected unit has an Eт capacity greater than the value just calculated.

STEP 5: Calculate the total energy per hour: ETC = ET x C
Extend $=6.91 \times 800=5,531 \mathrm{Nm} / \mathrm{hr}$
Retract $=4.97 \times 800=3,976 \mathrm{Nm} / \mathrm{hr}$
Use the Shock Absorber Specification Chart to verify that the selected unit has and ETC capacity greater that the value calculated.
STEP 6: Determine the damping constant required
Using the appropriate Shock Absorber performance graph, locate the intersection point for impact velocity ( V ) and total energy ( E ). The area ( -2 or -3 ) that the point falls in is the correct damping constant for the application.
Unit should be ordered with -NE3-NR2 options or select shock 67127-01-3 for extend and shock 67127-01-2 for retract.

## SHOCK ABSORBER SELECTION GUIDE: SERIES STP

## SIZING EXAMPLE: VERTICAL APPLICATION

## IMPERIAL

STEP 1: Application Data Example: STPD125 x 2 -AE1-NE1x-NRx with a 30 lb payload on extend and 1 lb on retract
A) $\mathrm{W}_{\mathrm{T}}=$ Total moving weight $=$ std moving + option adder + load
Extend $=2.6 \mathrm{lb}+.29 \mathrm{lb}+.29 \mathrm{lb}+30 \mathrm{lb}=33.18 \mathrm{lb}$ Retract $=2.6 \mathrm{lb}+.29 \mathrm{lb}+.29 \mathrm{lb}+1 \mathrm{lb}=4.18 \mathrm{lb}$


METRIC

## STEP 1: Application Data

Example: STPD525 x 50 -AE1-NE1x-NRx
with a 133 N payload on extend and 4.4 N on retract
A) $\mathrm{W}_{\mathrm{T}}=$ Total moving weight $=$ std moving + option adder + load
Extend $=11.6 \mathrm{~N}+1.29 \mathrm{~N}+1.29 \mathrm{~N}+133 \mathrm{~N}=147.18 \mathrm{~N}$
Retract $=11.6 \mathrm{~N}+1.29 \mathrm{~N}+1.29 \mathrm{~N}+4.4 \mathrm{~N}=18.58 \mathrm{~N}$
B) Velocity at impact: $V_{E}=25 \mathrm{in} / \mathrm{sec}$ (extend), $V_{R}=20 \mathrm{in} / \mathrm{sec}$ (retract)
C) Number of cycles/hour: $\mathrm{C}=800 \mathrm{cycles} / \mathrm{hr}$
D) Application type: Vertical
E) Operating pressure: 80 psi

STEP 2: Calculate the kinetic energy
$\mathrm{EK}_{\mathrm{K}}=.5 \times \mathrm{W}_{\mathrm{m}} \times \mathrm{V}^{2} / 386$
Extend $=.5 \times 33.18 \times 25^{2} / 386=26.9 \mathrm{in}$ - lb
Retract $=.5 \times-4.18 \times 20^{2} / 386=-2.2$ in-lb (working against gravity)
Note: -AR option could replace-NRx option
STEP 3: Calculate the propelling force and work energy
$\mathrm{FD}=$ (Effective Piston Area $\times$ Operating Pressure) $\pm$ Wtm
Extend $=(1.52 \times 80)+30=151.6 \mathrm{lb}$ (working with gravity)
Retract $=(1.17 \times 80)-4.18=89.42 \mathrm{lb}$ (working against gravity)
Use the Shock Absorber Specification Chart to verify that the selected unit has an FG capacity greater than the value just calculated.
$\mathrm{E} w=\mathrm{FD} \times \mathrm{S}$
Extend $=151.6 \times .448=67.9 \mathrm{in}-\mathrm{lb}$
Retract $=89.42 \times .448=40.1 \mathrm{in}-\mathrm{lb}$
STEP 4: Calculate the total energy: $\mathrm{ET}_{\mathrm{T}}=\mathrm{E}_{\mathrm{K}}+\mathrm{Ew}$
Extend $=26.9+67.9=94.8 \mathrm{in}-\mathrm{lb}$
Retract $=-2.2+40.1=37.9 \mathrm{in}-\mathrm{lb}$
Use the Shock Absorber Specification Chart to verify that the selected unit has an Er capacity greater than the value just calculated.
STEP 5: Calculate the total energy per hour: $\mathrm{ETC}=\mathrm{Et} \times \mathrm{C}$
Extend $=94.8 \times 800=75,840 \mathrm{in}-\mathrm{lb} / \mathrm{hr}$
Retract $=37.9 \times 800=30,320 \mathrm{in}-\mathrm{lb} / \mathrm{hr}$
Use the Shock Absorber Specification Chart to verify that the selected unit has and ETC capacity greater that the value calculated.
STEP 6: Determine the damping constant required
Using the appropriate Shock Absorber performance graph, locate the intersection point for impact velocity ( V ) and total energy ( E ). The area ( -2 or -3 ) that the point falls in is the correct damping constant for the application.
Unit should be ordered with -NE12-NR2 options or select shock 67127-01-2 for extend and shock 67127-01-2 for retract.
B) Velocity at impact: $\mathrm{V}_{\mathrm{E}}=.64 \mathrm{~m} / \mathrm{sec}$ (extend),
$\mathrm{V}_{\mathrm{R}}=.51 \mathrm{~m} / \mathrm{sec}$ (retract)
C) Number of cycles/hour: C=800 cycles/hr
D) Application type: Vertical
E) Operating pressure: 5.5 bar

STEP 2: Calculate the kinetic energy
日K $=.5 \times$ Wtm $\times \mathrm{V}^{2} / 9.8$
Extend $=.5 \times 147.18 \times .64^{2} / 9.8=3.08 \mathrm{Nm}$
Retract $=.5 \times-18.58 \times .51^{2} / 9.8=-.25 \mathrm{Nm}$ (working against gravity)
Note: -AR option could replace-NRx option
STEP 3: Calculate the propelling force and work energy
$\mathrm{FD}=$ (Effective Piston Areax Operating Pressure x .1 ) $\pm \mathrm{W}_{\mathrm{Tm}}$
Extend $=(982 \times 5.5 \times .1)+147.18 \mathrm{~N}=673 \mathrm{~N}$ (working with gravity)
Retract $=(756 \times 5.5 \times .1)-18.58 \mathrm{~N}=397 \mathrm{~N}$ (working against gravity)
Use the Shock Absorber Specification Chart to verify that the selected unit has an FG capacity greater than the value just calculated.
$\mathrm{E} w=\mathrm{FD} \times \mathrm{S}$
Extend $=673 \times .0114=7.67 \mathrm{Nm}$
Retract $=397 \times .0114=4.53 \mathrm{Nm}$
STEP 4: Calculate the total energy: $\mathrm{E}_{\mathrm{T}}=\mathrm{Ek}_{\mathrm{k}}+\mathrm{Ew}_{\mathrm{w}}$
Extend $=3.08+7.67=10.75 \mathrm{Nm}$
Retract $=-.25+4.53=4.28 \mathrm{Nm}$
Use the Shock Absorber Specification Chart to verify that the selected unit has an Er capacity greater than the value just calculated.
STEP 5: Calculate the total energy per hour: ETC = Et x C
Extend $=10.75 \times 800=8600 \mathrm{Nm} / \mathrm{hr}$
Retract $=4.28 \times 800=3424 \mathrm{Nm} / \mathrm{hr}$
Use the Shock Absorber Specification Chart to verify that the selected unit has and ETC capacity greater that the value calculated.
STEP 6: Determine the damping constant required
Using the appropriate Shock Absorber performance graph, locate the intersection point for impact velocity ( V ) and total energy ( E ). The area ( -2 or -3 ) that the point falls in is the correct damping constant for the application.
Unit should be ordered with -NE12-NR2 options or select shock 67127-01-2 for extend and shock 67127-01-2 for retract.


[^0]:    * TOLERANCEIS $\pm .001$ BETWETN DOWE PIN HOLES.

